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This chapter describes the environmental setting and study area for groundwater; analyzes impacts that could result from construction, operation, and maintenance of the project; and provides mitigation to reduce the effects of impacts. This chapter also analyzes the impacts on groundwater resources that could result from implementation of compensatory mitigation required for the project and analyzes the impacts that could result from the mitigation measures proposed in other resource chapters in this Draft Environmental Impact Report (Draft EIR).

8.0 Summary Comparison of Alternatives

Table 8-0 provides a summary comparison of anticipated impacts by alternative, as described in Chapter 3, *Description of the Proposed Project and Alternatives*, on groundwater. This table provides information on the magnitude of the most pertinent and quantifiable impacts on groundwater that are expected to result from operation of the project alternatives, and is based on quantitative analyses conducted to assess impacts on groundwater levels, groundwater storage, and interconnected surface water flows. The table presents the CEQA findings after all mitigation is applied. A regional scale integrated groundwater and surface water model, called the Delta Groundwater (DeltaGW) model (see Section 8.3, *Groundwater Impacts*), was used as the analytical tool for quantitative analysis of impacts on groundwater from project operations. The impacts on groundwater from construction and maintenance are discussed qualitatively, as are impacts related to groundwater quality and inelastic land subsidence resulting from groundwater pumping.

The DeltaGW Model simulation results and associated evaluations (including those for qualitative assessments) indicate that no significant groundwater impacts are expected to occur as a result of project operations. All groundwater impacts are under established thresholds for each impact area. There are slight changes in stream losses/gains, groundwater elevations, and groundwater in storage resulting from project operations, but these changes are less than significant and often within the margin of error for the model simulation results. However, during project construction and maintenance, there is a potential for impacts due to temporary localized changes in groundwater elevations from dewatering at construction and maintenance sites. These localized impacts could affect water wells near the project sites, cause changes in groundwater elevation to mobilize existing contaminant plumes, or result in the migration of lower-quality groundwater into areas of higher-quality groundwater. Implementation of Mitigation Measure GW-1: *Maintain Groundwater Supplies in Affected Areas* during construction and maintenance would ensure localized impacts on groundwater resources would be avoided.

Impacts resulting in increases in agricultural drainage due to project construction and operations are considered to be less than significant. Implementation of Mitigation Measure GW-5: *Increases in Groundwater Elevations Near Project Intake Facilities Affecting Agricultural Drainage*, would further reduce risks of impacts on agricultural drainage.

1 **Table 8-0. Comparison of Impacts of Project Operations on Groundwater by Alternative**

Groundwater Impact Mechanism	Alternative								
	1	2a	2b	2c	3	4a	4b	4c	5
Impact GW-1: Changes in Stream Gains or Losses in Various Interconnected Stream Reaches (%)	-0.82% LTS	-1.19% LTS	-0.64% LTS	-0.67% LTS	-0.85% LTS	-1.21% LTS	-0.64% LTS	-0.77% LTS	-0.81% LTS
Impact GW-2: Changes in Groundwater Elevations	0 LTS	0 LTS	0 LTS	0 LTS	0 LTS	0 LTS	0 LTS	0 LTS	0 LTS
Impact GW-3: Reduction in Groundwater Levels Affecting Supply Wells	0 LTS	0 LTS	0 LTS	0 LTS	0 LTS	0 LTS	0 LTS	0 LTS	0 LTS
Impact GW-4: Changes to Long-Term Change in Groundwater Storage (AF/acre)	0.017 LTS	0.03 LTS	0.01 LTS	0.015 LTS	0.016 LTS	0.029 LTS	0.01 LTS	0.014 LTS	0.024 LTS
Impact GW-5: Increases in Groundwater Elevations near Project Intake Facilities Affecting Agricultural Drainage (%)	+0.06% LTS	+0.10% LTS	+0.09% LTS	+0.04% LTS	+0.08% LTS	+0.12% LTS	+0.11% LTS	+0.06% LTS	+0.07% LTS
Impact GW-6: Damage to Major Conveyance Facilities Resulting from Land Subsidence	LTS	LTS	LTS	LTS	LTS	LTS	LTS	LTS	LTS
Impact GW-7: Degradation of Groundwater Quality	LTS	LTS	LTS	LTS	LTS	LTS	LTS	LTS	LTS

2 LTS = less than significant.

8.1 Environmental Setting

This section describes the environmental setting and affected environment for groundwater in the study area that may be influenced by the Delta Conveyance Project or project alternatives.

For the purposes of this analysis, the groundwater study area (the area in which groundwater impacts may occur) primarily consists of the Delta region, shown in Figure 1-1 in Chapter 1, *Introduction*. The project footprint (the conveyance facilities, Southern Forebay, intakes, and Bethany Complex) is within this region. Quantitative analysis of groundwater impacts due to project operations was conducted only for the Delta region. The study area, as defined in Chapter 1, also includes two other regions: (1) Upstream of the Delta region and (2) south-of-Delta State Water Project (SWP) services area region. Impacts on groundwater basins upstream of the Delta region are not included in this chapter because flow changes in those areas resulting from project construction and operation are negligible and are unlikely to cause changes in groundwater. Potential groundwater impacts on groundwater basins south of the Delta are only discussed qualitatively in this chapter. Groundwater impacts on both the Delta and south-of-Delta portions of the study area were evaluated herein because construction effects could occur in the Delta near the construction sites, and operations effects could occur throughout the Delta as well as in the south-of-Delta portions of the Central Valley that use SWP and Central Valley Project (CVP) water as a large portion of their water portfolio (see Chapter 6, *Water Supply*, for further discussion). Many groundwater systems are physically interconnected with surface waters flowing through those groundwater basins; these systems are also discussed in Chapter 5, *Surface Water*, and Chapter 6.

8.1.1 Study Area

The Delta and the Central Valley overlie several extensive groundwater basins that play key roles in local and regional water supply. Rivers draining the Coast Ranges, the Cascade Ranges, and the Sierra Nevada convey water into the Central Valley, interconnect with the underlying groundwater basins, and eventually flow into the Sacramento–San Joaquin Delta and San Francisco Bay. The study area evaluated in this chapter includes the Central Valley groundwater subbasins (both within the Delta and immediately south of the Delta) that could potentially be directly affected by project construction and operations.

Private individual groundwater wells and wells operated by community water agencies provide most of the residential potable water sources for several of the Delta communities, such as Clarksburg, Courtland, Freeport, Hood, Isleton, Rio Vista, Ryde, and Walnut Grove. The largely agricultural San Joaquin Valley uses groundwater to support agricultural and municipal demands (Chapter 6). Some water flowing to and through the Delta is diverted by local Sacramento users (e.g., the cities of Sacramento and Folsom), by users adjacent to or downstream of the Delta (e.g., Contra Costa Water District [CCWD]), and/or exported by the SWP/CVP to areas outside the Delta (Chapter 6). The availability of these surface water supplies influences the groundwater use and conditions of those export service areas.

Throughout the study area, hydrogeology and hydrology strongly influence groundwater flow and aquifer recharge with natural conditions affected by local land and water use. The existing groundwater conditions in the study area are briefly described in Section 8.3, *Groundwater Impacts*, to support discussions of environmental consequences associated with construction of project

1 alternatives, as well as other impacts on groundwater resources stemming from the long-term
2 operations and maintenance of the project facilities.

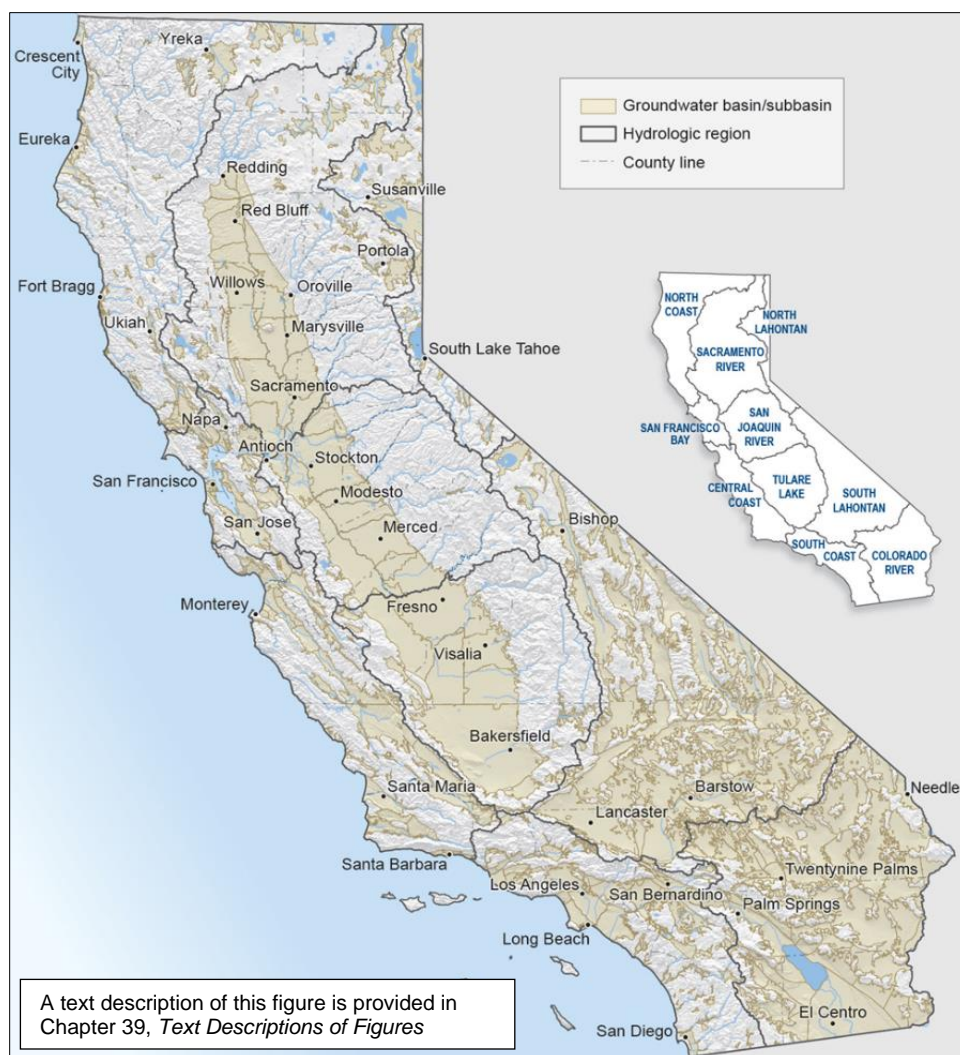
3 **8.1.2 Central Valley Groundwater**

4 Groundwater is a vital resource in California. It accounts for 41% of the state's total average annual
5 water supply and up to 58% of the total annual water supply in drought years. About 83% of
6 Californians depend on groundwater for some portion of their water supply and many communities
7 are 100% reliant on groundwater for all their water needs (California Department of Water
8 Resources 2021:H-1). The importance of groundwater as a resource varies regionally. The Central
9 Valley of California is the biggest user of groundwater in California with 78% of total statewide
10 groundwater use occurring within its borders. In the Central Valley, groundwater represents 53% of
11 the total water supply on an average annual basis, with the Tulare Lake Hydrologic Region meeting
12 about 69% of its local uses with groundwater and the rest of the Central Valley meeting between
13 15% and 35% of local uses with groundwater. The Central Coast Hydrologic Region has the highest
14 reliance on groundwater to meet its local uses, with more than 90% of its water use supplied by
15 groundwater in an average year. In Southern California, groundwater meets between 15% and 37%
16 of annual use (South Coast Hydrologic Region) and 40% of annual use (South Lahontan Hydrologic
17 Region) (California Department of Water Resources 2021:H-16).

18 During droughts, California has historically depended more heavily upon groundwater.
19 Groundwater resources will not be immune to climate change; in fact, historical patterns of
20 groundwater recharge have changed considerably. Because droughts are expected to be exacerbated
21 by climate change, efficient groundwater basin management will be necessary to avoid additional
22 overdraft and to take advantage of opportunities to store water underground and eliminate existing
23 overdraft.

24 **8.1.2.1 Groundwater Basins and Subbasins**

25 The California Department of Water Resources (DWR) has delineated 515 distinct alluvial
26 groundwater basins in the state as shown in Figure 8-1 and described in California's Groundwater
27 Update 2020 (California Department of Water Resources 2021:2-4). These basins and subbasins
28 have varying degrees of supply reliability depending on basin yield, storage capacity, and water
29 quality. Outside the Delta, to the north, the Sacramento River watershed overlies the Sacramento
30 Valley groundwater basin; to the south, the San Joaquin River watershed overlies the San Joaquin
31 Valley basin. The Delta region overlies groundwater subbasins from both the Sacramento Valley and
32 San Joaquin Valley groundwater basins.



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Figure 8-1. California's Groundwater Basin and Hydrologic Regions

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The large and diverse Sacramento Valley and San Joaquin Valley groundwater basins have been subdivided into groundwater subbasins based primarily on geologic features (e.g., faults, rock-type contacts), hydrologic features (e.g., rivers), or jurisdictional boundaries (e.g., county lines) (California Department of Water Resources 2021:2-11). The individual groundwater subbasins are not hydraulically distinct from others within a particular basin and may have a high degree of interconnection with neighboring basins. Where connected, the subbasins tend to behave as a single extensive alluvial Central Valley aquifer system.

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The Sacramento Valley groundwater basin extends from the Red Bluff Arch south to the Cosumnes River and underlies portions of Tehama, Glenn, Butte, Yuba, Colusa, Placer, Sutter, Solano, Sacramento, and Yolo Counties. The Red Bluff Arch is near the northern end of the Central Valley and separates the Sacramento Valley groundwater basin from the Redding Area groundwater basin. The southern portion of the Sacramento Valley groundwater basin underlies the northern portion of the Delta. The Sacramento Valley groundwater basin is extremely productive and provides much of the water supply for California's agricultural and urban water needs.

1 The San Joaquin Valley groundwater basin underlies the entire San Joaquin Valley, from the south at
2 the Tehachapi Mountains to the north with its boundary with the Sacramento Valley, where the
3 basin's northern portion underlies the southern half of the Delta. Two hydrologic regions occur in
4 the San Joaquin Valley groundwater basin: the San Joaquin River and the Tulare Lake Hydrologic
5 Regions. Overall, the groundwater basin is continuous, but the surface water regime affects local
6 groundwater conditions. The agricultural area of the San Joaquin Valley is heavily dependent upon
7 groundwater and surface water deliveries south of the Delta to support agricultural and municipal
8 demands. According to DWR estimates, more than half of all groundwater use in the state occurs in
9 the San Joaquin Valley groundwater basin (California Department of Water Resources 2021:H-9),
10 and this use has increased in past years as permanent crops (predominantly fruit and nut trees)
11 replace truck (annual) crops and dry grazing. This recent increase in demands to meet the water
12 needs of permanent crops has resulted in increased overdraft conditions and land subsidence
13 resulting from pumping below the Corcoran Clay layer (a regional aquitard). All but three of the
14 groundwater subbasins in the San Joaquin Valley groundwater basin have been deemed to be in
15 critical overdraft condition under the Sustainable Groundwater Management Act of 2014 (SGMA).

16 Outside the Delta watershed, other areas that receive surface water from the Delta watershed
17 include the Central Coast Hydrologic Region and portions of Southern California and the San
18 Francisco Bay Area region, which have more hydraulically distinct groundwater basins than the
19 Central Valley. Here too, many of the groundwater basins on the Central Coast and in Southern
20 California have been either adjudicated to address past overdraft conditions or classified as critically
21 overdrafted under SGMA.

22 **8.1.2.2 Groundwater–Surface Water Interaction**

23 Rivers play a large role in the hydrogeology of the Central Valley by bringing water from the uplands
24 during the snowpack's spring melt and providing recharge to the underlying aquifers. In areas of
25 shallow groundwater tables, rivers also can receive groundwater inflow. The quantity and timing of
26 snowpack melt are the predominant factors affecting surface water and groundwater, with peak
27 runoff typically following peak precipitation by 1 to 2 months (U.S. Geological Survey 1991:A2).
28 Rivers drain the Coast Ranges and the Sierra Nevada, bringing the water into the valley and
29 converging with the Sacramento and San Joaquin Rivers aligned along the axes of their respective
30 valleys (see Chapter 5). The drainage in each valley has a key difference: in the San Joaquin Valley,
31 fewer major streams drain the Coast Ranges, whereas the Sacramento Valley has several, including
32 Stony, Cache, Putah Creeks, and numerous other westside tributary creeks that flow to the
33 Sacramento River.

34 In the Sacramento Valley groundwater basin, the interaction between surface water and
35 groundwater systems is highly variable spatially and temporally. Generally, the major trunk streams
36 of the valley (the Sacramento and Feather Rivers) tend to act as drains and receive groundwater
37 discharge throughout most of the year. The exceptions are areas of depressed groundwater levels
38 attributable to groundwater pumping, where the water table has been artificially lowered, inducing
39 leakage from the rivers that recharge the groundwater system. In contrast, the tributary streams
40 draining into the Sacramento River from upland areas are almost all *losing* streams (water from the
41 streams enters and recharges the groundwater system) in their upper reaches, but some transition
42 to *gaining* streams (water from the groundwater enters the streams) farther downstream, closer to
43 their confluences with the Sacramento River. Groundwater modeling studies of the Sacramento
44 Valley suggest that, on average, the flux of groundwater discharging to the rivers is approximately
45 equal to the quantity of water that leaks from streams to recharge the aquifer system. The studies

1 suggest that, in average years, stream recharge and aquifer recharge are each about 800,000 acre-
2 feet per year (AFY) (Glenn Colusa Irrigation District and the Natural Heritage Institute 2010:8-15-8-
3 17).

4 In the San Joaquin Valley groundwater basin, the interaction between the surface water and
5 groundwater systems is substantially different. Long-term groundwater production throughout this
6 basin has lowered groundwater levels beyond what natural recharge can replenish. Most streams
7 leak to the underlying aquifers and recharge the aquifer system. For example, along much of the San
8 Joaquin River, the river is a losing river and groundwater is recharged by leakage from the river.
9 This is especially true in the Gravelly Ford area of the San Joaquin River (upstream of Mendota
10 Pool), where the riverbed is highly permeable and river water readily seeps into the underlying
11 aquifer. In the northern portions of the San Joaquin Valley groundwater basin, groundwater levels
12 are shallow adjacent to the river and groundwater discharges into the river (McBain and Trush
13 2002:4-17-4-23).

14 The San Joaquin River has three major tributaries that flow from the east: the Merced, Tuolumne,
15 and Stanislaus Rivers. The Cosumnes, Mokelumne, and Calaveras Rivers also flow into the San
16 Joaquin River where the river joins the tidally influenced Delta. These rivers and many of their
17 tributaries are, for the most part, losing streams in their upper reaches but in some cases transition
18 to gaining streams closer to their confluence with the San Joaquin River (State Water Resources
19 Control Board 2012:9-9). Streams draining from the Coast Ranges on the west side are ephemeral
20 and are predominantly losing streams along their entire length.

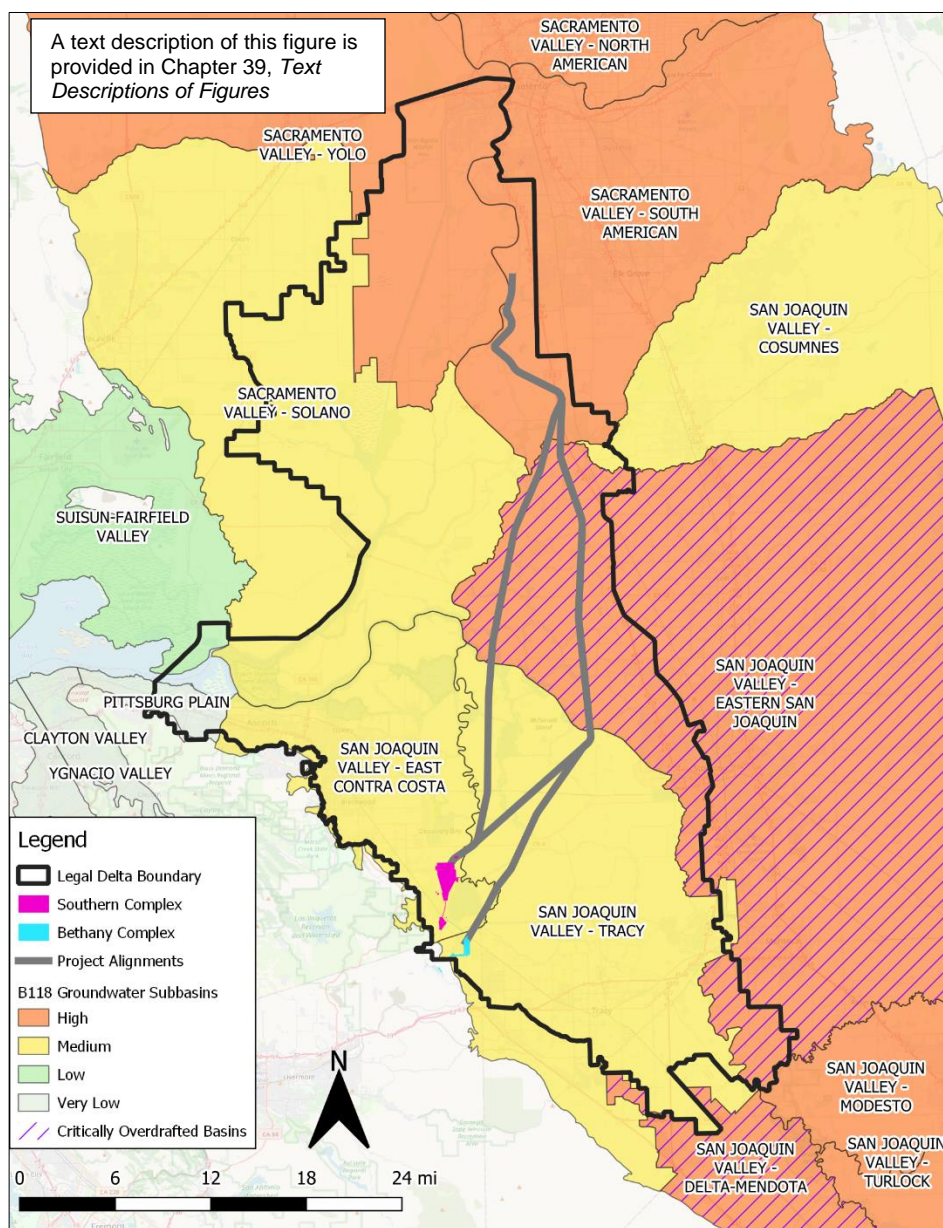
21 Historically, rivers have defined the boundaries for most groundwater subbasins in the Sacramento
22 and San Joaquin Valleys. However, in almost all cases, these rivers do not act as hydraulic barriers or
23 groundwater divides. An example is Putah Creek, which delineates the boundary between the
24 Sacramento Valley groundwater basin's Yolo and Solano Subbasins (California Department of Water
25 Resources 2004a:1). As Putah Creek flows eastward through Solano and Yolo Counties toward the
26 Sacramento River, numerous diversions along its course reduce streamflow to minimal levels by the
27 time it reaches the Sacramento River. As the creek passes through the Yolo Bypass, which has no
28 well-defined channel, the potential for the creek to act as a hydraulic barrier between the subbasins
29 is further reduced. Although the groundwater system in the Yolo Bypass has not been well studied, it
30 is likely that it functions as a single alluvial aquifer rather than the two discrete aquifers as the
31 official subbasin (Yolo and Solano) designations suggest.

32 The major regional aquifers that make up the Sacramento Valley and San Joaquin Valley
33 groundwater basins are regionally extensive aquifer systems. These aquifer systems act as large
34 interconnected alluvial aquifers that may be subdivided vertically but are not isolated local-scale
35 aquifer systems as one might infer from the subbasin terminology.

36 **8.1.3 Delta Region Groundwater**

37 The Delta region overlies the western portion of the study area where the Sacramento Valley and
38 San Joaquin Valley groundwater basins converge. Underlying the northern Delta, within the
39 Sacramento Valley groundwater basin, are the Solano Subbasin in the northwest and the South
40 American Subbasin to the northeast, bounded by the Sacramento and Cosumnes Rivers. Within the
41 San Joaquin Valley groundwater basin, the Tracy Subbasin underlies the southern half of the Delta,
42 and the Eastern San Joaquin and Cosumnes Subbasins underlie the central and eastern Delta as
43 shown in Figure 8-2.

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3 **Figure 8-2. Groundwater Basins underlying the Delta Region**

4 Physical and hydrogeologic characterizations of each major groundwater basin underlying the Delta
 5 can be found in DWR's *California's Groundwater*—Bulletin 118 (California Department of Water
 6 Resources 2003, 2016), California Water Plan Groundwater Update (California Department of Water
 7 Resources 2015), various U.S. Geological Survey reports (U.S. Geological Survey 1960, 2006:8,
 8 2008:6), and other available literature as cited throughout this chapter.

9 The groundwater basins in the state are assigned a basin priority—high (including critically
 10 overdrafted), medium, low, very low—under the provisions of the SGMA. The high- and medium-
 11 priority groundwater basins were required to form groundwater sustainability agencies (GSA) and
 12 develop and implement groundwater sustainability plans (GSP) to achieve sustainability within 20

1 years from initial deadline for submission of GSPs. Figure 8-2 shows that the Delta region overlies
2 portions of the critically overdrafted Eastern San Joaquin Subbasin and several high- and medium-
3 priority subbasins.

4 **8.1.3.1 Groundwater Basin Hydrogeology**

5 In general, shallow groundwater conditions and extensive groundwater-surface water interaction
6 characterize the Delta area. Spring runoff generated by melting snow in the Sierra Nevada increases
7 flows in the Sacramento and San Joaquin Rivers and tributaries and causes groundwater levels near
8 the rivers to rise. Because the Delta is a large floodplain and the shallow groundwater is
9 hydraulically connected to the surface water, changes in river stages affect groundwater levels and
10 vice versa. This hydraulic connection is also evident when the tide is high and surface water flows
11 from the ocean into the Delta, thereby increasing groundwater levels nearby.

12 Groundwater levels in the central Delta are very shallow, and land surface elevations have dropped
13 on several islands resulting in groundwater levels close or above the ground surface in many areas.
14 Maintaining groundwater levels below crop rooting zones is critical for successful agriculture,
15 especially for islands that lie below sea level, and many farmers rely on an intricate network of
16 drainage ditches and pumps to maintain groundwater levels of about 3 to 6 feet below ground
17 surface (bgs). The accumulated agricultural drainage is pumped through or over the levees and
18 discharged into adjoining streams and canals (U.S. Geological Survey 2000).

19 Delta floodplain deposits contain a significant percentage of organic material (peat), ranging in
20 thickness from 5 to 40 feet in the proposed conveyance alignments. Below the surficial deposits,
21 unconsolidated non-marine sediments occur above the fresh/saline water interface at depths as
22 shallow as a few hundred feet near the Coast Range to nearly 3,000 feet near the eastern margin of
23 the basin. These non-marine sediments form the major water-bearing formations in the Delta.
24 Groundwater in the South American and Eastern San Joaquin Subbasins generally flows from the
25 Sierra Nevada in the east toward the low-lying lands of the Delta to the west.

26 Groundwater levels in the South American Subbasin have fluctuated over the past 40 years, with the
27 lowest levels occurring during periods of drought. In general, flat to rising water levels mostly occur
28 within the west-central area of the South American Subbasin in the vicinity of the cone of depression
29 near Elk Grove that has been present for many years and along the American River (Sacramento
30 Central Groundwater Authority 2016:2-50). Falling water levels occur in the northeastern portion of
31 the subbasin in the vicinity of three groundwater remediation projects, including the Aerojet
32 Superfund Site, the U.S. Air Force Mather Field Superfund Site, and the McDonnell Douglas 29
33 Inactive Rancho Cordova Test Site at Mather Field and south of Security Park. Numerous
34 groundwater production wells west of these remediation projects also produce groundwater
35 (Sacramento Central Groundwater Authority 2016:2-50). Areas affected by municipal pumping
36 show a lower groundwater recovery level than other areas (California Department of Water
37 Resources 2004b:2). Groundwater levels in the Eastern San Joaquin Subbasin have continuously
38 declined in the past 40 years due to groundwater pumping. Cones of depression are present near
39 major pumping centers such as Stockton and Lodi (Eastern San Joaquin Groundwater Authority
40 2019). Groundwater level declines of up to 100 feet have been observed in some wells.

41 In the Solano Subbasin, the historical general groundwater flow direction is from northwest to
42 southeast (California Department of Water Resources 2004c:1). Increasing agricultural and urban
43 development in the 1940s in the Solano Subbasin caused groundwater level declines. Today,

1 groundwater levels are mostly affected by drought cycles but tend to recover quickly during wet
2 years (California Department of Water Resources 2004c:2).

3 In the Tracy Subbasin, groundwater generally flows south to north and discharges into the San
4 Joaquin River. According to DWR and the San Joaquin County Flood Control and Water Conservation
5 District, groundwater levels in the Tracy Subbasin have been relatively stable over the past 10 years,
6 apart from seasonal variations resulting from recharge and pumping, and declines in the
7 southeastern portion of the subbasin (California Department of Water Resources 2006:2; GEI
8 Consultants 2021:5-2).

9 **8.1.3.2 Groundwater Quality**

10 A groundwater quality study was performed in the southern Sacramento Valley region in which
11 more than 60 wells were sampled (U.S. Geological Survey 2008:13). As part of the Groundwater
12 Ambient Monitoring Assessment (GAMA) program, two wells were sampled in the Delta area. One is
13 located in the central Delta, west of Sherman Island and the Sacramento River, and has a depth of
14 800 feet bgs. The other well is located in the eastern Delta, near the Delta Cross Channel, and has a
15 depth of 244 feet bgs. Both wells were sampled for several chemical constituents. Some of the
16 results from this study are reported in this section along with results from other studies and reports.

17 In the South American Subbasin, total dissolved solids (TDS) levels range from 24 to 581 milligrams
18 per liter (mg/L), with an average of 221 mg/L based on 462 records (California Department of
19 Water Resources 2004b:3). Seven sites present significant groundwater contamination in this basin,
20 including three Superfund sites near the Sacramento metropolitan area. These sites are in various
21 stages of cleanup. Between 2009 and 2018, the most commonly detected chemicals above a primary
22 maximum contaminant level (MCL) or secondary maximum contaminant level (SMCL) in the South
23 American Subbasin were manganese (42%), iron (21%), and arsenic (16%) (California Department
24 of Water Resources 2021). These percentages are for when detections above MCLs or SMCLs occur.
25 Most samples did not report chemicals above their respective maximum levels.

26 TDS varies more widely in the Eastern San Joaquin Subbasin, ranging between 50 and 3,520 mg/L.
27 The high salinity of groundwater is attributed to poor-quality groundwater intrusion from the Delta
28 caused by the decline of groundwater levels and worsened by sea level rise. This saline groundwater
29 front has been particularly apparent in the Stockton area since the 1970s (San Joaquin County Flood
30 Control and Water Conservation District 2008:vii). Other possible sources of salinity in the subbasin
31 include Delta sediments, deep saline groundwater, and irrigation return water (Eastern San Joaquin
32 Groundwater Authority 2019).

33 High chloride concentrations have also been observed in well water in the Eastern San Joaquin
34 Subbasin. Chloride concentrations in 2017 are generally less than 150 mg/L, with some higher
35 measurements reaching 2,000 mg/L (Eastern San Joaquin Groundwater Authority 2019:2-55). In
36 addition, large areas of groundwater with elevated nitrate concentrations exist in several portions of
37 the subbasin, such as southeast of Lodi and south of Stockton. The City of Lodi operates the White
38 Slough Water Pollution Control Facility, a 6.3 million gallon per day (average flow) plant on the
39 eastern edge of the Delta, on the western side of Interstate (I-) 5, approximately 1 mile south of
40 Highway 12. Agricultural and stormwater runoff are returned to unlined holding ponds. Water
41 quality concerns have been evaluated regarding elevated nitrates and salinity by the State Water
42 Resources Control Board (City of Lodi 2006:19; Stockton Record Staff 2009; Eastern San Joaquin
43 Groundwater Authority 2019).

1 Between 2009 and 2018, the most commonly detected chemicals above an MCL or SMCL in the
2 Eastern San Joaquin Subbasin were manganese (16%), arsenic (16%), and iron (15%) (California
3 Department of Water Resources 2021). These percentages are for when detections above MCLs or
4 SMCLs occur. Most samples did not report chemicals above their maximum levels.

5 Groundwater quality in the Solano Subbasin is generally good and is deemed appropriate for
6 domestic and agricultural use (California Department of Water Resources 2004c:3). However, TDS
7 concentrations at levels higher than 500 mg/L have been observed in the central and southern areas
8 of the basin. Between 2009 and 2018, the most commonly detected chemicals above an MCL or
9 SMCL in the Solano Subbasin were manganese (29%), arsenic (26%), and iron (21%) (California
10 Department of Water Resources 2021). These percentages are for when detections above MCLs or
11 SMCLs occur. Most samples did not report chemicals above their maximum levels.

12 In the Tracy Subbasin, areas of poor water quality exist throughout. Elevated chloride
13 concentrations are found along the western side of the subbasin near the city of Tracy and along the
14 San Joaquin River. Between 2009 and 2018, the most commonly detected chemicals above an MCL
15 or SMCL in the Tracy Subbasin were arsenic (20%), manganese (18%), and iron (18%) (California
16 Department of Water Resources 2021). These percentages are for when detections above MCLs or
17 SMCLs occur. Most samples did not report chemicals above their maximum levels.

18 In the East Contra Costa Subbasin, groundwater quality generally meets most water quality
19 objectives and serves domestic and agricultural uses. Naturally occurring salinity levels are elevated
20 basin-wide and nitrate levels are slightly elevated in the shallow zone (less than 150 feet bgs). TDS
21 varies widely across the subbasin, although it is characteristically high, ranging between 500 and
22 1,500 mg/L in all areas. Chloride concentrations in the subbasin exceed or are near the
23 recommended SMCL for chloride (250 mg/L) in most wells, suggesting that water concentrations
24 are naturally higher for chloride. Nitrate is observed in some areas of the subbasin (i.e., Brentwood),
25 with concentrations exceeding the MCL (10 mg/L) that may be linked to historical agricultural
26 influences in the area. Arsenic concentrations are generally less than the MCL (10 micrograms per
27 liter) basin-wide, and boron concentrations are high in most wells and are attributed to a naturally
28 elevated baseline. Between 2009 and 2018, the most commonly detected chemicals above an MCL or
29 SMCL in the East Contra Costa Subbasin were manganese (36%), TDS (16%), and arsenic (7%)
30 (California Department of Water Resources 2021). These percentages are for when detections above
31 MCLs or SMCLs occur. Most samples did not report chemicals above their maximum levels.

32 **8.1.3.3 Groundwater Production and Use**

33 Groundwater is used throughout the Delta through the mechanisms of pumping and plant uptake in
34 the root zone. However, an accurate accounting of groundwater used in the region is not available
35 because most wells are not metered or otherwise reported in a reliable manner. In the upland
36 peripheral Delta areas, average annual groundwater pumping is estimated to range between
37 100,000 and 150,000 acre-feet (AF), both for domestic and agricultural uses (CALFED Bay-Delta
38 Program 2000:5.4-8). Although information on groundwater yield is limited in the Delta subbasins,
39 available estimates in the northern San Joaquin Valley groundwater basin indicate that maximum
40 well yield varies from around 1,500 to 3,000 gallons per minute (gpm).

41 The Stockton metropolitan area uses groundwater in conjunction with surface water for its
42 municipal and industrial water needs. CCWD does not use groundwater to meet any demands,
43 though within CCWD's service area, groundwater is pumped by industries, private individuals, and

1 public municipal utilities including the cities of Martinez and Pittsburg, Golden State Water
2 Company, and Diablo Water District (Contra Costa Water District 2016:6-1). It is estimated that
3 these users can pump approximately 6,500 AFY based on available pumping records and land-use-
4 based estimates. An undetermined number of privately owned groundwater wells exist in the CCWD
5 service area (CALFED Bay-Delta Program 2005:3-6). Groundwater in this area is primarily produced
6 from the Clayton groundwater basin, which has seen gradual declines in groundwater elevation
7 (Contra Costa Water District 2005:18).

8 Groundwater also provides water supply for the Delta communities of Clarksburg, Courtland,
9 Freeport, Hood, Isleton, Rio Vista, Ryde, and Walnut Grove. In the rural portions of the Delta, private
10 groundwater wells provide domestic water supply (Solano Agencies 2005). In the central Delta,
11 groundwater use is limited because of low well yields and poor water quality. Shallow groundwater
12 occurring at depths of less than 100 feet is too saline and therefore not adequate for most beneficial
13 uses. Approximately 200 square miles of the central Delta are affected by saline shallow
14 groundwater (CALFED Bay-Delta Program 2000:5.4-7). Because shallow groundwater levels are
15 detrimental when they encroach on crop root zones, groundwater pumping is used to drain the
16 waterlogged agricultural fields. Groundwater pumping for agricultural irrigation mostly occurs in
17 the north Delta for orchards and in the south Delta around the city of Tracy.

18 **8.1.3.4 Land Subsidence**

19 Declining land surface elevations in the Delta are well documented and a major source of concern
20 for farming operations. The oxidation of peat soils is the primary mechanism of sinking lands in the
21 Delta (U.S. Geological Survey 2000), and some areas are below sea level (see Chapter 11, *Soils*, and
22 Chapter 10, *Geology and Seismicity*). In portions of the San Joaquin Valley groundwater basin, drops
23 in land surface elevations have occurred as a result of excessive groundwater pumping, below the
24 Corcoran Clay (a regional aquitard) or below other regionally significant clay layers (the
25 predominant mechanism for subsidence in this area). Land subsidence occurs as the result of the
26 compression of the Corcoran Clay and other fine-grained units where groundwater that supports
27 the aquifer framework has been removed by pumping.

28 **8.2 Applicable Laws, Regulations, and Programs**

29 The applicable laws, regulations, and programs considered in the assessment of project impacts on
30 groundwater are indicated in this section, in Section 8.3.1, *Methods for Analysis*, or the impact
31 analysis, as appropriate. Applicable laws, regulations and programs associated with state and
32 federal agencies that have a review or potential approval responsibility have also been considered in
33 the development CEQA impact thresholds or are otherwise considered in the assessment of
34 environmental impacts. A listing of some of the agencies and their respective potential review and
35 approval responsibilities, in addition to those under CEQA, is provided in Chapter 1, *Introduction*,
36 Table 1-1. A listing of some of the federal agencies and their respective potential review, approval,
37 and other responsibilities, in addition to those under NEPA, is provided in Chapter 1, Table 1-2.
38 Federal laws and regulations that address water quality may also apply to groundwater quality, as
39 presented in Chapter 9, *Water Quality*, and Chapter 11, *Soils*, including the Clean Water Act, National
40 Pollutant Discharge Elimination System (NPDES) Program Antidegradation Policy (40 Code of
41 Federal Regulations [CFR] § 131.6); Clean Water Act, Nonpoint Source Management Program (33
42 United States Code [USC] § 1329); Clean Water Act, Municipal Separate Storm Sewer Systems policy

1 (40 CFR § 122.34 and § 122.26(d); and Safe Drinking Water Act (42 USC §§ 300f–300j-26). These
2 regulations are federally mandated and implemented in California through the State Water
3 Resources Control Board. State regulations that address water quality may also apply to
4 groundwater quality, including the Order No. 2009-0009-DWQ, NPDES General Permit No.
5 CAS000002, Waste Discharge Requirements for Discharges of Stormwater Runoff Associated with
6 Construction as presented in Chapter 9 and Chapter 11. The State has also mapped
7 Hydrogeologically Vulnerable Areas, defined by the State Water Resources Control Board in 2000 in
8 response to Executive Order D-5-99.

9 **8.3 Groundwater Impacts**

10 This section describes the direct and cumulative impacts associated with groundwater that would
11 result from project construction and operation (including maintenance). Measures to mitigate (i.e.,
12 avoid, minimize, rectify, reduce, eliminate, or compensate for) significant impacts, if any, are also
13 discussed in this section. Indirect impacts are discussed in Chapter 31, *Growth Inducement*.

14 **8.3.1 Methods for Analysis**

15 The groundwater analysis addresses two different aspects of the project. First, the analysis
16 addresses changes in groundwater conditions in the vicinity of the project facilities in the Delta
17 resulting from construction activities. Second, the analysis addresses changes in groundwater
18 conditions in the Delta region resulting from project operations.

19 The Delta Conveyance Project construction- and maintenance-related effects were evaluated
20 qualitatively due to the lack of an available analytical tool at the spatial scale required for the site-
21 specific quantitative analysis. The Delta Groundwater Model used for the quantitative groundwater
22 analysis is a regional-scale model with an average element size of 0.57 square mile. Project facilities
23 have a footprint, which is an order of magnitude smaller than the average element size of the model.
24 Furthermore, the model grid was adapted from an existing model (see Section 8.3.1.1, *Analysis Tool:*
25 *Delta Groundwater Model*) and was not configured to align with the project facilities. The qualitative
26 evaluations are based on existing groundwater conditions and hydrogeology and anticipated
27 changes in groundwater elevations, storage, and quality from the construction methods and
28 protocols described in *Volume 1: Delta Conveyance Final Draft Engineering Project Report—Central*
29 *and Eastern Options* and *Volume 1: Delta Conveyance Final Draft Engineering Project Report—*
30 *Bethany Reservoir Alternative* (Engineering Project Reports) (Delta Conveyance Design and
31 Construction Authority 2022a, 2022b). On the other hand, the effects of project operations on
32 groundwater conditions were evaluated quantitatively using the DeltaGW Model, a numerical
33 integrated groundwater surface water model described in Appendix 8A, *Delta Groundwater Model:*
34 *Development and Calibration*. The groundwater study area is the area within the DeltaGW Model
35 domain, which covers the valley floor area between the Bear River and Cache Creek in the north and
36 the Tuolumne River in the south. It includes the southern subbasins of the Sacramento Valley
37 groundwater basin (including the Yolo, Solano, and North American Subbasins) and the northern
38 subbasins of the San Joaquin Valley groundwater basin (including the South American, Tracy, East
39 Contra Costa, Cosumnes, and Eastern San Joaquin Subbasins). The quantitative analysis of effects of
40 project operations includes evaluation of resultant changes in groundwater elevations (including
41 associated effects on supply wells and agricultural drainage systems), groundwater storage, and
42 interconnected surface water systems.

1 The effects of project operations on land subsidence and groundwater quality resulting from
2 changes in groundwater conditions were also evaluated qualitatively due to the lack of an available
3 analytical tool. Finally, impacts on and benefits to the Delta export service areas were addressed
4 qualitatively as the DeltaGW Model area overlies only the area containing project infrastructure and
5 does not include Delta export service areas.

6 **8.3.1.1 Analysis Tool: Delta Groundwater Model**

7 To facilitate quantitative groundwater analyses, a new integrated groundwater-surface water
8 model, called the DeltaGW Model, was developed. The model was used to evaluate the effects of the
9 long-term operation of the water conveyance facilities associated with the project on groundwater
10 resources in the Delta region. As previously noted, construction impacts were evaluated
11 qualitatively and were not included in the DeltaGW Model analysis.

12 The DeltaGW Model is based on DWR's Integrated Water Flow Model platform (California
13 Department of Water Resources 2021) and simulates land surface processes, groundwater flows,
14 surface water flows, and stream aquifer interactions in response to stresses from water use, land
15 use, and hydrologic variability. The DeltaGW Model utilizes the same model grid structure as the
16 C2VSim-FG model, but covers a smaller model domain that includes the Delta and surrounding areas
17 (Figure 8-3). Model nodes and elements of C2VSim-FG within the DeltaGW Model domain are
18 renumbered to maintain independence from C2VSim-FG. Initially, relevant model input data from
19 C2VSim-FG were mapped to the renumbered grid and element set of the DeltaGW Model. Later,
20 geologic, hydrologic, and land and water use data were enhanced with available recent data from
21 various local and regional sources, including calibrated local models within the DeltaGW Model
22 domain. New boundary conditions were also developed for the northern and southern boundaries of
23 the DeltaGW Model domain. The DeltaGW Model layering is also enhanced to create a six-layer
24 model compared to the four-layer C2VSim-FG model.

25 The DeltaGW Model is a completely independent and separate model from C2VSim-FG. The DeltaGW
26 Model was calibrated with enhanced data and aquifer layering for a historical period from 1974 to
27 2015 on a monthly timestep. A detailed description of model development and calibration is
28 provided in Appendix 8A, *Delta Groundwater Model: Development and Calibration*.

29 The DeltaGW Model domain is subdivided laterally into variably sized elements over a 4,834-
30 square-mile area with an average element size of 0.57 square mile. The model has 8,459 elements
31 and 7,977 nodes, with an equivalent average area of 0.6 square mile per node. The aquifer
32 underlying the model domain is divided vertically into six layers with variable thicknesses to a
33 maximum thickness of 2,900 feet. The top three layers are 65, 50, and 50 feet thick respectively, for
34 a total thickness of 165 feet, which generally corresponds to the bottom of the project tunnel.

35 The DeltaGW Model domain is divided into five model subregions for the purpose of analysis, as
36 shown in Figure 8-3. Model subregion 4 represents the Delta region, the primary focus of
37 quantitative analysis of project operations. This subregion contains the project footprint of
38 conveyance tunnels, the project intakes, the Southern Forebay, and the Bethany Complex. Within
39 each of these subregions, the DeltaGW Model simulates agricultural demand components,
40 representing crop irrigation requirements, urban demands based on population and per capita
41 water use, and the supply components representing surface water deliveries and estimated
42 groundwater pumping to meet the water demands. The model generates monthly groundwater
43 elevations at each of the model nodes.

1



2

3 **Figure 8-3. DeltaGW Model Domain and Model Subregions**

4 **8.3.1.2 Approach for Analysis**

5 The analysis methodologies describe the potential impacts on groundwater resources from
 6 construction and long-term operations activities associated with the project alternatives. The
 7 analyses rely upon geospatial information identifying temporary ground-disturbing activities
 8 necessary for project construction in the study area. Longer-term effects resulting from the physical
 9 footprints of water conveyance facilities and conservation areas, as well as operational effects on
 10 groundwater resources, are described separately. Areas south of the Delta that receive Delta water
 11 would not be affected during construction activities in the Delta because the changes in
 12 groundwater levels resulting from construction dewatering occur locally around the site of

1 dewatering and do not affect other groundwater basins. During construction activities, the Delta
2 exports are assumed to remain identical to what they would be without construction activities
3 associated with the new conveyance facility.

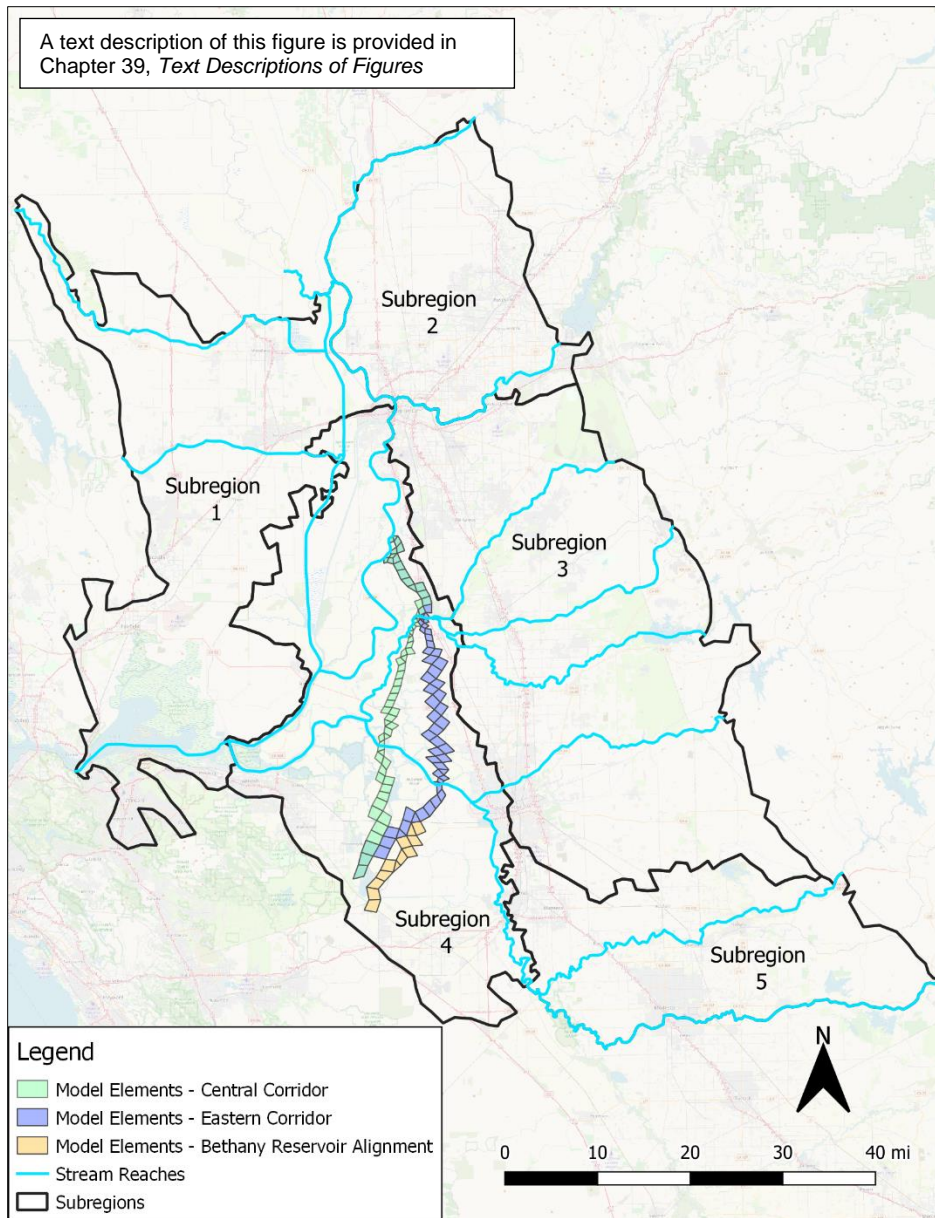
4 Impacts on groundwater resources from project operations as they relate to stream-aquifer
5 interactions, groundwater levels, hydraulic gradients, and/or the quantity of groundwater in storage
6 were evaluated quantitatively utilizing the DeltaGW Model, which covers the Delta region and
7 adjacent groundwater basins, not the entire Central Valley. As a result, the geographic scope of the
8 quantitative analysis of groundwater impacts of the project does not include the entire Central
9 Valley or areas south of the Delta. At the initiation of this groundwater study, the C2VSim-FG was
10 not available as a fully calibrated model, nor were there uniform models of the Central Coast and
11 Southern California groundwater basins. Therefore, groundwater impacts on areas south of Delta
12 are discussed qualitatively in this chapter. In addition, the results of the DeltaGW Model simulations
13 indicate very limited groundwater-related impacts due to project operations; hence, little to no
14 groundwater-related impacts are anticipated in the Central Valley outside the DeltaGW Model
15 domain, upstream of Delta or south of Delta.

16 **Use of the DeltaGW Model for Evaluation of Impacts of Project Operations**

17 The DeltaGW Model was used to evaluate the operational impacts of project alternatives against the
18 existing (baseline) conditions. Operations are considered over a 94-year simulation period utilizing
19 hydrology from 1922 through 2015. Model stresses for the existing condition and project alternative
20 model runs utilize data from the CalSim 3 model used in the surface water analysis (see Chapter 5,
21 *Surface Water*, and Chapter 6, Section 6.4.1, *Methods for Analysis*, for further descriptions of the
22 assumptions associated with CalSim 3 modeling). Land use, precipitation, evapotranspiration,
23 irrigation periods, and urban demands were all assigned in the DeltaGW Model using the same input
24 data as used in the CalSim 3 model. Surface water flows, diversions, Delta exports, and project
25 operations under existing conditions and the alternatives were obtained from the results of the
26 CalSim 3 analyses and used as input data for the DeltaGW Model. Changes in surface water deliveries
27 unrelated to the Delta Conveyance Project diversions between existing conditions and project
28 alternatives as simulated by the CalSim 3 model for surface water analyses are reflected in the
29 DeltaGW Model. These changes are considered to be a part of the project operational impacts. The
30 physical features of the project are modeled for each alternative as low-permeability model
31 elements whose alignments are shown in Figure 8-4. Each project alternative is simulated in
32 DeltaGW with the combination of intakes and tunnel corresponding to the alternative; as a result,
33 only one conveyance alignment is ever simulated at a time in the DeltaGW Model. Surface water
34 elevation changes occurring in the Southern Forebay are not simulated in the DeltaGW Model
35 because the forebay is not expected to have substantive interactions with the underlying aquifers
36 due to perpetual forebay inundation to a minimum of several feet of water depth. The existing
37 condition in the DeltaGW Model does not include any of the project features. The comparison of the
38 project alternatives against existing conditions reflects differences in groundwater conditions
39 resulting from the physical features of the project (e.g., tunnel and intakes), project operations, and
40 any other changes in flow or surface water diversions expected as a result of the project.

41 In this analysis, each project alternative is compared to existing conditions (the CEQA baseline) to
42 quantitatively analyze groundwater level changes and associated impacts in the Delta that are
43 caused by operation of the alternative. Detailed modeling assumptions and results are documented
44 in Appendix 8B, *Impact Analysis: Groundwater Model Results*.

1 In addition to project alternatives, the DeltaGW Model was also used to compare the 2040 No
 2 Project Alternative against the 2020 existing condition (CEQA baseline). The 2040 No Project
 3 Alternative leverages the same underlying data and assumptions used for the No Project Alternative
 4 surface water analysis conducted in CalSim 3, which assumes that the only projects constructed
 5 under the No Project Alternative are those built without the Delta Conveyance Project. The DeltaGW
 6 modeling analysis did not include other projects explicitly. The DeltaGW model incorporates land
 7 use, precipitation, evapotranspiration, irrigation periods, and urban demands data from the CalSim
 8 3 inputs and the surface water flows and diversions from the CalSim 3 outputs. The 2040 No Project
 9 Alternative is compared against the existing conditions (CEQA baseline) to evaluate changes in
 10 groundwater conditions resulting from climate change, land use, and demand changes under future
 11 conditions.
 12



13
 14 **Figure 8-4. DeltaGW Model Physical Project Components**

1 **Analysis of Groundwater Conditions Upstream of the Delta Region**

2 Groundwater basins underlying the Sacramento Valley are recharged directly through precipitation
3 and irrigation recharge and through the interconnected surface water courses (e.g., Sacramento,
4 Yuba, and Feather Rivers) that run through or adjacent to them. While groundwater is used for both
5 potable and irrigation supply, in most areas of the Sacramento Valley, groundwater levels recover to
6 pre-irrigation season levels each spring. As noted in Chapter 6, *Water Supply*, upstream reservoir
7 storage and river flows do not substantially change between the project alternatives and the existing
8 conditions when operation of the project alternatives are simulated. For Trinity Lake, Shasta Lake,
9 Lake Oroville, and Folsom Lake, storage changes are extremely minimal. In some cases, there are
10 very minor increases in end-of-September storage because of lower releases for exports (because of
11 diversions at the proposed north Delta intakes) and carriage water savings. Additionally, as noted in
12 Chapter 5, *Surface Water*, the long-term average of monthly flows and average monthly flows by
13 water year type on the Sacramento River (a key interconnected surface water course in the
14 Sacramento Valley) as simulated in CalSim 3 under all project alternatives would be similar when
15 compared to existing conditions. As project impacts on upstream interconnected surface water
16 courses are anticipated to be minimal, the resultant impacts on groundwater upgradient from the
17 Delta are also anticipated to be minimal as a result of project operations.

18 Given the nominal changes in surface water flows and storage in the large upstream reservoirs and
19 the need to utilize a refined flow model (the DeltaGW Model) in the study area to evaluate for
20 impacts immediately adjacent to project infrastructure, the Sacramento Valley groundwater basins
21 and areas upstream of Bear River are not evaluated in this chapter.

22 **Analysis of Groundwater Conditions in South-of-Delta SWP Service Areas**

23 Operations of the Delta Conveyance Project would stabilize surface water deliveries in the south-of-
24 Delta SWP service areas, as described in Chapter 6. Average annual SWP deliveries would increase
25 from existing conditions under all project alternatives for the long-term average, dry years, and
26 critical water years. SWP Table A and Article 56 deliveries are expected to increase under the long-
27 term average, dry years, and critical water years compared to deliveries under existing conditions.
28 Average annual SWP Article 21 deliveries would also increase under the long-term average and,
29 depending on the alternative, would decrease or increase under dry and critical water years. Article
30 21 deliveries typically include a small amount for north-of-Delta SWP water contractors that could
31 occur every year and occasional but more significant deliveries for south-of-Delta contractors. The
32 project alternatives are not likely to affect the frequency of north-of-Delta Article 21 deliveries but
33 could influence, and likely increase, those for south-of-Delta deliveries.

34 Longer-term averages show increases in San Luis Reservoir storage across all project alternatives.
35 The project is not expected to affect San Joaquin River flows nor the operations of reservoirs south
36 of the Delta on the tributaries of the San Joaquin River (e.g., CVP Millerton Lake on the San Joaquin
37 River and the New Melones Reservoir on the Stanislaus River); therefore, neither locations and
38 reservoirs on the San Joaquin River (and tributaries) nor San Joaquin Valley groundwater subbasins
39 were evaluated further. Appendix 5A, *Modeling Technical Appendix*, includes flows for additional
40 locations and storage for additional reservoirs within the study area (that are not relevant to the
41 discussion in this chapter).

1 **Thresholds of Significance**

2 The effects of a project alternative on groundwater would be significant under CEQA if
3 implementation of the alternative would result in one of the potential impacts described in this
4 section based on the general questions posed in the CEQA Guidelines Appendix G Environmental
5 Checklist. The thresholds of significance are also discussed below for these potential impacts.

- 6 ● **Impact GW-1: Changes in Stream Gains or Losses in Various Interconnected Stream**
7 **Reaches**—Changes in stream gains/losses are considered substantial if the annual increase in
8 stream losses to the groundwater system or the annual decrease in stream gains from the
9 groundwater system for the major streams in the Delta region would be more than 5% with
10 respect to the annual average stream aquifer gains/losses under existing conditions (CEQA
11 baseline) in the corresponding streams. The 5% threshold is deemed reasonable because it is
12 small relative to the historical variations in annual stream gains/losses, which ranges from 62%
13 to 124% of average annual stream gains/losses over the historical period from 1974 to 2015 in
14 stream reaches in the Delta region (Appendix 8A). Annual values are used in assessing impacts
15 on stream gains/losses because groundwater response to streamflow changes is a relatively
16 slow process.
- 17 ● **Impact GW-2: Changes in Groundwater Elevations**—Groundwater elevation changes
18 resulting from project operations in the study area are considered substantial if these changes
19 are significantly higher than historical groundwater elevation changes. Historical data for the
20 1974–2015 period from 132 wells in the Delta region (model subregion 4) shows that
21 groundwater elevations fluctuate and have deviated from the mean values at wells by more than
22 5 feet (rise or fall) about 23% of the time and by more than 15 feet (rise or fall) about 5% of the
23 time. Therefore, it is conservative to consider changes in groundwater elevations to be
24 significant when greater than +/-5 feet of change in groundwater elevations occurs more than
25 5% of the time due to project operations. Short-term (less than 5% of the time) fluctuations in
26 groundwater elevations are not considered significant because the groundwater elevations
27 recover before causing any impact.
- 28 ● **Impact GW-3: Reduction in Groundwater Levels Affecting Supply Wells**—Reduced
29 groundwater levels could affect the capacity of the supply wells and may result in some
30 shallower wells going dry or requiring well modifications such as the lowering of pump intakes.
31 A review of well completion reports from DWR’s Online System of Well Completion Reports
32 (OSWCR) database shows a total of 3,565 production wells were installed within the statutory
33 Delta boundary between 1977 and 2018. These wells have a median depth of 190 feet and an
34 average depth of 211 feet. Reduction in groundwater levels is considered substantial if more
35 than 20 feet of groundwater decline occurs at a supply well in the Delta region. The 20-foot
36 groundwater decline threshold for supply wells is deemed to be a conservative estimate for
37 depletion of groundwater supplies because it is less than 10% of the average depth of supply
38 wells in the statutory Delta.
- 39 ● **Impact GW-4: Changes to Long-Term Change in Groundwater Storage**—Groundwater
40 storage changes in the Central Valley vary widely—annual reduction has been estimated to be
41 between 900 thousand acre-feet (TAF) and 2,100 TAF from 2006 to 2018 (California
42 Department of Water Resources 2021:6-17). Based on the calibrated DeltaGW historical (1974–
43 2015) model, annual changes in groundwater storage in the Delta region varies widely from -
44 214 TAF (decrease) to 253 TAF (increase) with a long-term change in storage of 1,170 TAF.
45 Historical fluctuations in annual change of storage are approximately 20% of the historical long-

1 term change in storage. Therefore, it is conservative to consider changes in long-term
2 groundwater storage to be substantial if there is more than a 5% difference in the change in
3 long-term storage compared to existing conditions in the Delta region.

- 4 • **Impact GW-5: Increases in Groundwater Elevations near Project Intake Facilities**
5 **Affecting Agricultural Drainage**—Agricultural drainage operations are common in most areas
6 of the Delta to lower groundwater levels to prevent impacts on the root zone of agricultural
7 crops. As such, only increases in groundwater levels are considered to have negative impacts on
8 agricultural drainage operations. It is assumed that existing drainage systems have sufficient
9 capacity for some increased volumes of drainage. Large-scale variations in agricultural drainage
10 (70%–150% of the average) were estimated based on the results of the historical calibrated
11 DeltaGW Model. Therefore, it is conservative to consider more than 10% increase in annual
12 agricultural drainage flows to be substantial.
- 13 • **Impact GW-6: Damage to Major Conveyance Facilities Resulting from Land Subsidence**—
14 Substantial and the persistent drop in long-term average groundwater elevations over a wide
15 area in the Delta region (model subregion 4) could result in groundwater-level-induced land
16 subsidence depending on the underlying geologic/hydrogeologic conditions. No quantitative
17 analysis of land subsidence impacts of the project was conducted because of the lack of
18 availability of land subsidence process modeling under project operations. Instead, the drops in
19 groundwater elevations near the major conveyance facilities obtained from the groundwater
20 flow model results were used to qualitatively infer potential for land subsidence due to project
21 operations.
- 22 • **Impact GW-7: Degradation of Groundwater Quality**—Substantial degradation of
23 groundwater quality or the substantial migration of groundwater contaminant plumes toward
24 major supply wells would be counter to the state’s Antidegradation Policy as stated in State
25 Board Resolution 68-16. No quantitative analysis of water quality impacts of the project was
26 conducted because of the lack of availability of a contaminant transport model to support
27 quantitative analysis. Instead, the changes in groundwater elevations around the known
28 contaminant plume sites obtained from the groundwater flow model results were used to
29 qualitatively infer potential for migration of plumes near the project alignment.

30 Evaluation of Mitigation Impacts

31 CEQA also requires an evaluation of potential impacts caused by the implementation of mitigation
32 measures. Following the CEQA conclusion for each impact, the chapter analyzes potential impacts
33 associated with implementing both the Compensatory Mitigation Plan (CMP) and the other
34 mitigation measures required to address with potential impacts caused by the project. Mitigation
35 impacts are considered in combination with project impacts in determining the overall significance
36 of the project. Additional information regarding the analysis of mitigation measure impacts is
37 provided in Chapter 4, *Framework for the Environmental Analysis*.

38 8.3.2 Groundwater Impacts and Mitigation Approaches

39 8.3.2.1 No Project Alternative

40 As described in Chapter 3, *Description of the Proposed Project and Alternatives*, CEQA Guidelines
41 Section 15126.6 directs that an EIR evaluate a specific alternative of “no project” along with its
42 impact. The No Project Alternative in this Draft EIR represents the circumstances under which the

1 project (or project alternative) does not proceed and considers predictable actions, such as projects,
2 plans, and programs, that would be predicted to occur in the foreseeable future if the Delta
3 Conveyance Project is not constructed and operated. This description of the environmental
4 conditions under the No Project Alternative first considers how groundwater could change over
5 time and then discusses how other predictable actions could affect groundwater.

6 **Future Groundwater Conditions**

7 Under the No Project Alternative, SWP/CVP operations are assumed to be similar to existing
8 conditions. It is expected that DWR and Reclamation would continue to operate the SWP and CVP to
9 divert, store, and convey water consistent with applicable laws, contractual obligations, and permit
10 requirements. This alternative also assumes no construction or modifications to SWP or CVP
11 facilities or operations criteria between 2020 and 2040 would occur, and the implementation of
12 GSPs developed in response to the SGMA, including associated projects for the sustainable
13 management of underlying groundwater basins.

14 Overall, groundwater conditions in the Delta, and SWP and CVP service areas would be expected to
15 vary under the No Project Alternative because of a variety of factors. Sea level rise, climate change,
16 an increase in north-of-Delta urban water demands, and changes in land use could be expected to
17 cause changes in SWP and CVP deliveries as compared to existing conditions, and could result in
18 associated changes in groundwater conditions as groundwater extractions may increase to make up
19 for shortages in surface water deliveries until the high- and medium-priority groundwater basins
20 are operated in compliance with SGMA. Additionally, the implementation of GSPs submitted in 2020
21 for critically overdrafted subbasins (predominantly in the San Joaquin Valley) and the anticipated
22 implementation of GSPs in noncritically overdrafted medium- and high-priority groundwater basins
23 (predominantly in the Sacramento Valley) could result in the development of new programs and
24 projects to achieve and maintain basin sustainability on a regional level, including the development
25 of new surface water supplies, new groundwater recharge projects, and in some places,
26 groundwater pumping curtailments. Implementation of the GSPs and the resulting achievement of
27 groundwater sustainability by 2040 or 2042 would result in stable groundwater levels and the
28 active management of groundwater extractions within predetermined operating ranges.

29 For a discussion of the potential responses of SWP and CVP water users to reduced SWP and CVP
30 deliveries, please refer to Chapter 3, *Description of the Proposed Project and Alternatives*, and
31 Appendix 3C, *Defining Existing Conditions, No Project Alternative, and Cumulative Impact Conditions*.
32 As explained therein, responses of urban water users could include water use efficiency measures,
33 increased reliance on groundwater, increased reliance on reservoir storage, contingency planning
34 efforts, increased use of recycled water, increased water transfers, increased reliance on
35 desalination as a water supply, and water use restrictions. Responses of agricultural water users
36 could include increased reliance on reservoir storage, managed aquifer recharge programs to
37 improve supply reliability, increased reliance on groundwater, land fallowing and/or conversion to
38 non-irrigated uses, and water conservation programs.

39 Historically, precipitation in most of California has been dominated by extreme variability over
40 seasonal, annual, and decadal timescales. In the context of climate change, projections of future
41 precipitation are even more uncertain and potentially variable than projections for temperature.
42 Uncertainty regarding precipitation projections is greatest in the northern part of the state, and a
43 stronger tendency toward drying is indicated in the southern part of the state. The projected
44 reduction in snowpack under climate change can significantly change the availability and pattern of

1 surface water resources because Sierra Nevada snowpack is the primary source of water supply and
2 natural groundwater recharge in California (California Department of Water Resources 2019:1-14).
3 Climate models project more extreme winter precipitation events that would be more in the form of
4 rain rather than snow; therefore, they would generate higher runoffs, creating additional flooding
5 concerns; and a more rapid spring snow melt, leading to shorter, more intense spring periods of
6 river flow and freshwater discharge. These changes in surface water hydrology will have a direct
7 impact on the timing and volume of recharge to the underlying groundwater basins. Sea level rise,
8 another anticipated impact resulting from climate change, could be expected to affect coastal
9 groundwater basins directly by driving seawater further inland in the subsurface, and groundwater
10 basins in and around the Delta indirectly by driving saltwater further inland in Delta surface water,
11 resulting in changes to surface water management and releases from upstream freshwater
12 reservoirs to offset the increased Delta water salinity levels.

13 The 2040 No Project Alternative was also compared against the existing conditions using the
14 DeltaGW Model to assess potential groundwater impacts that could occur in the absence of the Delta
15 Conveyance Project under future conditions. The 2040 No Project Alternative model run of the
16 DeltaGW Model utilizes the same underlying hydrology and demand data used in the surface water
17 analysis for the 2040 No Project scenario in CalSim 3 (see Chapter 5, *Surface Water*, and Chapter 6,
18 *Water Supply*, for further description of the assumptions associated with CalSim 3 modeling). Water
19 supplies and demands in the 2040 No Project Alternative in CalSim differ from existing conditions in
20 order to represent project changes in land use, urban growth, climate change, and sea level rise.

21 The 2040 No Project Alternative DeltaGW Model scenario utilizes 2040 land use developed for the
22 California Water Plan Update 2013, 2040 urban demands based on 2015 urban water management
23 plans and population data, and precipitation and evapotranspiration under a climate change
24 assumption. The simulation period considers 94 years of hydrology (from 1922 through 2015).
25 Twenty global climate projections were developed and used to perturb historical observed
26 meteorological data to develop the 2040 climate dataset. The meteorological data were used in
27 developing unimpaired rim water inflows as well as evapotranspiration associated with agricultural
28 and managed wetland water demands. Land use data are based on a future scenario developed for
29 DWR for the California Water Plan, Update 2013, which assumes that recent trends would continue
30 into the future.

31 The modeled 2040 No Project Alternative assumes construction and operation of the notched
32 Fremont Weir, but does not include any other projects that could occur in the absence of the Delta
33 Conveyance Project. The 2040 No Project Alternative does include the projects that would move
34 forward in the absence of the Delta Conveyance Project. However, the modeled representation of the
35 2040 No Project Alternative does not include those projects because of their programmatic nature.
36 Furthermore, only projects that are implemented within the DeltaGW Model domain could be
37 included in the analysis. Potential projects under SGMA are not considered as part of this analysis.
38 As a result, modeled groundwater changes occurring under the 2040 No Project Alternative when
39 compared with 2020 existing conditions are predominantly due to climate change conditions and
40 expected changes to land use, agricultural, and urban demands. These changes are presented below
41 in the same categories of changes in groundwater resources listed in *Thresholds of Significance* in
42 Section 8.3.1.2, *Approach for Analysis*, to facilitate understanding of the responses of groundwater
43 system under the 2040 climate change scenario. A detailed description of modeling assumptions is
44 provided in Appendix 8B.

1 **Increase in Stream Losses in Various Interconnected Stream Reaches**

2 Without the project in place, changes to streamflow are dictated by climate change and 2040 level of
3 development. Under 2040 No Project conditions, the Sacramento River, San Joaquin River, and
4 Suisun Bay (the three major interconnected stream courses in the study area) would see a small
5 increase in stream losses to groundwater compared to the existing conditions. The Sacramento
6 River would see a reduction in stream losses, while the San Joaquin River and Suisun Bay would see
7 an increase in losses. This change is caused by the increased gradient between the stream stage and
8 underlying groundwater elevation under 2040 conditions. Long-term average monthly flows during
9 the winter and spring generally increase due to altered inflow patterns as a result of climate change,
10 with more precipitation falling as rain rather than snow, and more extreme winter precipitation
11 events. Between May and October, flows decrease as a result of climate change with diminished
12 snow accumulation and an earlier snowpack melt. The resulting changes in streamflow, coupled
13 with the influence of sea level rise, result in higher average stream stage in the San Joaquin River
14 and Suisun Bay compared to existing conditions. Increased evapotranspiration and greater urban
15 water demands result in greater groundwater use and lower groundwater elevations across the
16 region. Overall, the stream losses would increase by less than 2% with respect to average annual
17 stream aquifer interaction under existing conditions in any water year for all three streams.

18 **Changes in Groundwater Elevation**

19 Under the 2040 No Project Alternative, climate change, land use, and urban demand changes would
20 result in increased pumping to compensate for the increase in water demands resulting from higher
21 future temperatures. Evapotranspiration is assumed to increase by approximately 5% under 2040
22 climate change conditions. Land use shifts to less water-intensive crops, and overall agricultural
23 water demand would decrease by 54 TAF across the DeltaGW Model domain. Surface water
24 deliveries for agriculture would remain mostly unchanged. Urban water demands would increase by
25 approximately 50% between existing conditions and 2040 conditions, from 841 TAF to 1,268 TAF
26 within the DeltaGW Model domain. While surface water deliveries for urban use would increase,
27 additional groundwater pumping would still occur to meet the increased demand. An increase of
28 122 TAF of average annual groundwater pumping would occur over the 94-year simulation period,
29 resulting in localized groundwater elevation declines of 50 to 60 feet in some areas of the DeltaGW
30 Model domain. The greatest increase in groundwater pumping and corresponding groundwater
31 elevation decline would occur over a limited area near the city of Fairfield as a result of increased
32 urban water demands. These declines are not the result of project operations as this is an analysis of
33 anticipated impacts on groundwater resources without the project.

34 **Reduction in Groundwater Levels Affecting Supply Wells**

35 Under the 2040 No Project Alternative, groundwater elevations in two Public Land Survey System
36 (PLSS) sections, or 20 (0.3%) of the 5,244 production wells evaluated in the DeltaGW Model, would
37 decline by more than 20 feet relative to the existing conditions. The groundwater declines would be
38 primarily a result of increased pumping to meet increased urban water demands and higher
39 agricultural water demands under climate change conditions and not as a result of project
40 operations. The maximum simulated groundwater decline at a production well would be about 25
41 feet near the city of Sacramento. However, the 2040 No Project Alternative does not explicitly
42 consider SGMA; it only considers land use/evapotranspiration changes based on current
43 trends/climate change and supply changes independent of SGMA. It is likely that there would be

1 demand reductions or supply augmentation under sustainable groundwater management that may
2 reduce the reported declines.

3 **Long-Term Declines of Groundwater in Storage**

4 In subregion 4 (i.e., the Delta region) of the DeltaGW Model, annual loss in groundwater storage
5 under the 2040 No Project Alternative is about 4,899 AFY relative to the existing conditions. This
6 change equates to an approximately 0.64 AF per acre reduction in groundwater storage across the
7 region at the end of the 94-year simulation period as compared to changes in groundwater storage
8 under existing conditions. This increased loss of groundwater in storage is a result of increased
9 groundwater use associated with higher agricultural and urban water demands in the Delta region
10 under 2040 conditions.

11 **Increases in Agricultural Drainage**

12 Agricultural drainage flows are expected to decrease under the 2040 No Project Alternative relative
13 to existing conditions primarily because of increased pumping to meet higher agricultural water
14 demands under climate change conditions. Overall, agricultural drainage would decrease under the
15 2040 No Project Alternative by 0.79% or 3,924 AFY relative to existing conditions.

16 **Damage to Major Conveyance Facilities from Land Subsidence**

17 Groundwater declines are expected to occur within the DeltaGW Model domain under the 2040 No
18 Project Alternative relative to existing conditions as a result of climate change, land use, and urban
19 demand changes. As described in the *Changes in Groundwater Elevation* section above, an increase of
20 122 TAF of average annual groundwater pumping would occur in the DeltaGW Model area over the
21 94-year simulation period, resulting in localized groundwater elevation declines in some areas of
22 the model domain. The greatest increase in groundwater pumping and corresponding groundwater
23 elevation decline of 50 to 60 feet would occur over a small (less than 3 square miles) area near the
24 city of Fairfield, near the model boundary, as a result of increased urban water demands under 2040
25 conditions. These declines are not the result of project operations because this is an analysis of
26 anticipated impacts on groundwater resources without the project. These groundwater declines
27 could potentially result in land subsidence, depending on how and where the groundwater is
28 extracted, and may result in damage to existing conveyance facilities in the study area.

29 **Degradation of Water Quality**

30 Degradation of water quality was not evaluated quantitatively; the changes in groundwater
31 elevations from the groundwater flow model were used for a qualitative evaluation of impacts.
32 Changes in groundwater elevations under the 2040 No Project Alternative relative to the existing
33 conditions are expected to occur as a result of climate change increasing water demands. Based on
34 groundwater flow model results, the largest groundwater elevation changes occur in urban areas
35 where demand increases are the most significant. Across the rest of the model domain, changes in
36 groundwater elevations would be less than 10 feet in most of the study area. These changes in
37 groundwater elevations could potentially change the flow of groundwater across the region enough
38 to mobilize contaminant plumes or cause migration of groundwater from areas of poor water
39 quality to areas of higher quality. Notably, the DeltaGW modeling analysis did not include effects of
40 sea level rise, which could contribute to saltwater intrusion in the Delta under 2040 conditions.

1 **Predictable Actions by Others**

2 A list and description of actions included as part of the No Project Alternative are provided in
 3 Appendix 3C, *Defining Existing Conditions, No Project Alternative, and Cumulative Impact Conditions*.
 4 As described in Chapter 4, *Framework for the Environmental Analysis*, the No Project Alternative
 5 analyses focus on identifying the additional water-supply-related actions public water agencies may
 6 opt to follow if the Delta Conveyance Project does not occur.

7 Public water agencies participating in the Delta Conveyance Project have been grouped into four
 8 geographic regions. The water agencies within each geographic region would likely pursue a similar
 9 suite of water supply projects under the No Project Alternative (see Appendix 3C, *Defining Existing*
 10 *Conditions, No Project Alternative, and Cumulative Impact Conditions*). At this time, it is assumed that
 11 the types of projects that are potentially feasible in each region could contribute to meeting
 12 demands in the face of further declines in reliable SWP supplies. Based on a review of the 2020
 13 urban and agricultural water management plans of the participating water agencies, Table 8-1
 14 summarizes the types of activities that could affect groundwater by state region in the No Project
 15 Alternative. Construction of water supply reliability projects and implementation of demand
 16 management measures would be needed to otherwise meet project objectives.

17 **Table 8-1. Examples of Effects on Groundwater from Construction and Operation of No Project**
 18 **Alternative Projects**

Project Type	Region(s) in Which Impact Would Likely Occur	Potential Groundwater Impacts
Increased/accelerated desalination	Northern coastal, southern coastal	<p><u>Potential Construction Impacts:</u> Temporary groundwater quality degradation as a result of the accidental release of hazardous construction chemicals if the construction areas are not properly managed through implementation of construction BMPs. Temporary reductions in groundwater elevations and/or storage if groundwater is used as a supply source during construction and/or if construction required dewatering.</p> <p><u>Potential Operations and Maintenance Impacts:</u> Long-term groundwater quality degradation from intrusion of saline waters as a result of onshore brackish groundwater extractions and/or potential increases in salinity of intruded groundwater.</p>
Groundwater recovery (brackish water desalination)	Northern inland, southern coastal, southern inland	<p><u>Potential Construction Impacts:</u> Temporary groundwater quality degradation as a result of the accidental release of hazardous construction chemicals if the construction areas are not properly managed through implementation of construction BMPs. Temporary reductions in groundwater elevations and/or storage if groundwater is used as a supply source during construction, if construction required dewatering, and/or as a result of groundwater extraction during well development and testing.</p> <p><u>Potential Operations and Maintenance Impacts:</u> Long-term groundwater quality degradation resulting from brine disposal via injection and/or near shore water discharge. Long-term reductions in groundwater elevations and/or storage resulting from the brackish groundwater extraction.</p>

Project Type	Region(s) in Which Impact Would Likely Occur	Potential Groundwater Impacts
Groundwater management	Northern coastal, northern inland, southern coastal, southern inland	<p><u>Potential Construction Impacts:</u> Temporary groundwater quality degradation as a result of groundwater discharges during well development and testing. Temporary reductions in groundwater elevations and/or storage if groundwater is used as a supply source during construction, if construction required dewatering, and/or as a result of groundwater extraction during well development and testing.</p> <p><u>Potential Operations and Maintenance Impacts:</u> Temporary groundwater quality degradation as a result of groundwater discharges during well maintenance. Long-term groundwater quality degradation as a result of the operation of groundwater recharge projects.</p>
Water recycling	Northern coastal, northern inland, southern coastal, southern inland	<p><u>Potential Construction Impacts:</u> Temporary groundwater quality degradation as a result of the accidental release of hazardous construction chemicals if the construction areas are not properly managed through implementation of construction BMPs. Temporary reductions in groundwater elevations and/or storage if groundwater is used as a supply source during construction and/or if construction required dewatering.</p> <p><u>Potential Operations and Maintenance Impacts:</u> None</p>
Water use efficiency measures	Northern inland, southern coastal, southern inland	<p><u>Potential Construction Impacts:</u> Temporary groundwater quality degradation as a result of groundwater discharges during well development and testing. Temporary reductions in groundwater elevations and/or storage if groundwater is used as a supply source during construction, if construction required dewatering, and/or as a result of groundwater extraction during well development and testing.</p> <p><u>Potential Operations and Maintenance Impacts:</u> None</p>

1 BMP = best management practice.
2

3 The project types in Table 8-1 are examples of water reliability projects that could occur if the Delta
4 Conveyance Project were not approved. Desalination projects are potentially feasible in the
5 northern and southern coastal regions. The southern coastal region might pursue larger and more
6 desalination projects than the northern coastal region to replace the water yield that otherwise
7 would have been received through the Delta Conveyance Project. Groundwater recovery (brackish
8 water desalination) is more feasible predominantly across the northern inland, southern coastal,
9 and southern inland regions. Groundwater management projects could occur in all regions, with
10 larger, more extensive management programs occurring in the northern inland areas. Water
11 recycling projects are less tied to any geographic feature and, therefore, could also be pursued in all
12 four regions. The northern inland region would require the fewest wastewater treatment/water
13 reclamation plants, followed by the northern coastal region and southern coastal region. The
14 southern inland region would require the most water recycling projects to replace the anticipated
15 water yield that would otherwise be received through the Delta Conveyance Project. Water

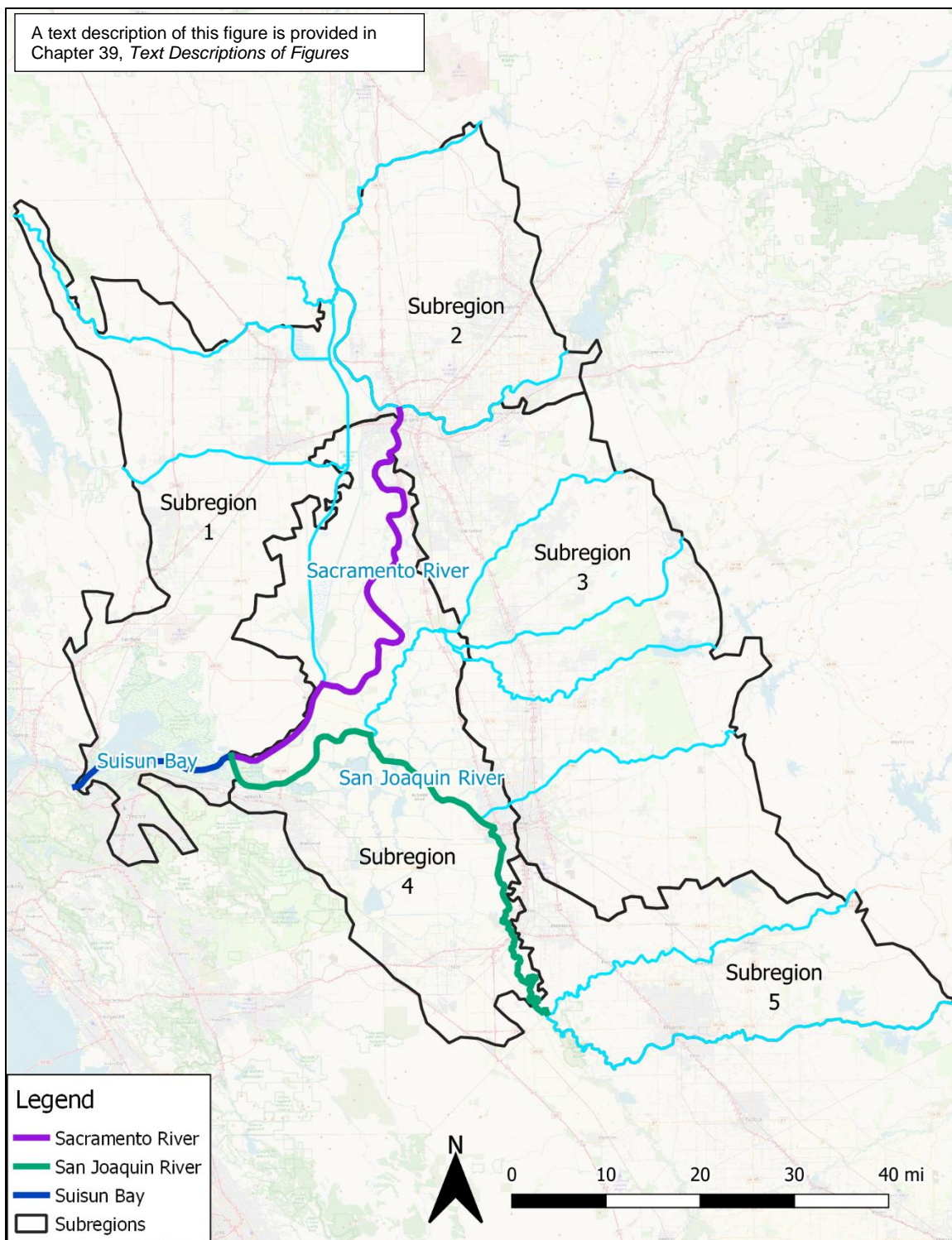
1 efficiency projects could be pursued in all four regions and involve a wide variety of project types,
2 such as flow measurement or automation in a local water delivery system, lining of canals, use of
3 buried perforated pipes to water fields, and the additional detection and repair of commercial and
4 residential leaking pipes. In general, impacts on groundwater from the construction of these
5 projects could include groundwater quality degradation as a result of the accidental release of
6 hazardous construction chemicals if the construction areas are not properly managed through
7 construction best management practices (BMPs) and/or groundwater discharges during well
8 development and testing. Construction impacts could also include the temporary reduction in
9 groundwater elevations and/or storage if groundwater is used as a supply source during
10 construction, if construction requires dewatering, and/or as a result of groundwater extraction
11 during well development and testing. Impacts on groundwater from operation of these other project
12 types include groundwater quality degradation resulting from brine disposal (either via injection or
13 as a result of near-shore ocean discharge) or the recharge of the groundwater basin with surface
14 water or stormwater and/or long-term reductions in groundwater elevations and/or storage
15 resulting from associated project groundwater extractions.

16 **8.3.2.2 Impacts of the Project Alternatives on Groundwater**

17 This section discusses changes to and associated impacts on groundwater resources from
18 construction and operation of the project alternatives relative to existing conditions. As mentioned
19 above, the DeltaGW Model results were used to evaluate the operational impacts of project
20 alternatives against the 2020 existing conditions. Construction practices are discussed in the
21 Engineering Project Reports (Delta Conveyance Design and Construction Authority 2022a, 2022b).

22 **Impact GW-1: Changes in Stream Gains or Losses in Various Interconnected Stream Reaches**

23 Changes in interconnected stream gains or losses are considered to be significant if they result in an
24 annual increase in stream losses to the groundwater system or an annual decrease in stream gains
25 from the groundwater system of more than 5% with respect to the average annual stream-aquifer
26 gains/losses under existing conditions (CEQA baseline). The three interconnected stream courses in
27 the study area considered herein to evaluate this impact are the Sacramento River reach from the
28 mouth of American River to the confluence of San Joaquin River; San Joaquin River reach from the
29 mouth of Stanislaus River to the confluence of Sacramento River; and Suisun Bay (Sacramento River
30 reach from the confluence with San Joaquin River to the outlet of the DeltaGW Model). Figure 8-5
31 shows these three stream reaches as simulated in the DeltaGW Model.



1
2

Figure 8-5. Interconnected Surface Water Reaches Analyzed in the DeltaGW Model

1 ***All Project Alternatives***

2 Changes in stream gains or losses as a result of project operations were evaluated by comparing
3 simulated stream gains or losses for each stream reach under existing conditions with those
4 simulated for each project alternative. Net changes to gains or losses across each river reach were
5 compared against the average annual stream-aquifer interaction in each river reach as a measure of
6 the likelihood of the project impacts on downstream and on ecological users of those watercourses.
7 Detailed simulation results can be found in Appendix 8B.

8 ***Project Construction***

9 Project construction under all project alternatives would not result in significant changes in
10 interconnected stream gains or losses as a result of construction activities. Project construction
11 would include the installation of slurry cutoff or sheet pile walls to reduce the potential for
12 dewatering impacts at the intakes and at the Southern Complex. The tunnel shafts would be “wet”
13 constructed such that the shaft walls would be slurry walls that prevent movement of groundwater.
14 The shaft would be constructed downward under wet conditions and the base would be formed
15 using concrete base “tremie plugs” that seal the bottom. Because the water would be removed from
16 a closed system within the tunnel shaft after the concrete liner and plug have been constructed, the
17 adjacent groundwater formations would not be affected during the dewatering of the shaft. No
18 dewatering would occur along the tunnel during tunnel boring.

19 The most substantial dewatering activities would occur at the intakes and Southern Forebay
20 Emergency Spillway (Delta Conveyance Design and Construction Authority 2022a, 2022b). At the
21 project intakes, deep cutoff walls would be constructed in the foundations of the sedimentation
22 basin, outlet channel perimeter embankment, and the temporary levee, as well as at the back of the
23 intake structure to isolate the internal subsurface from surrounding local groundwater for both
24 construction and operations phases. Additionally, piezometers would be installed outside the slurry
25 wall to allow monitoring of potential groundwater level impacts during construction for
26 management of dewatering activities. If required to mitigate potential impacts, Mitigation Measure
27 *GW-1: Maintain Groundwater Supplies in Affected Areas* could be implemented in which a series of
28 groundwater recharge and extraction wells could be installed around the external perimeter of the
29 intake cutoff wall system to allow discharge of captured dewatered water back into the subsurface
30 on the external side of the deep cutoff walls in the event that some local external effects due to
31 dewatering are observed. Conversely, these wells could be used to extract mounded water for return
32 to the sedimentation basins if needed to maintain local groundwater levels during construction and
33 operations.

34 Dewatering at the Southern Complex would occur during construction at the Southern Forebay
35 Emergency Spillway, Southern Forebay Outlet Structure, and the Outlet and Control Structures west
36 of Byron Highway (for Alternatives 1, 2a, 2b, 2c, 3, 4a, 4b, and 4c) and at the Delta-Mendota Control
37 Structure (for Alternatives 2a and 4a). Dewatering at the Southern Forebay Emergency Spillway,
38 adjacent to Italian Slough, would occur for several months. Sheet pile walls would be used to limit
39 impacts on groundwater levels from dewatering at the Southern Forebay Spillway and Southern
40 Forebay Outlet. Dewatering at the Outlet and Control Structures west of Byron Highway and the
41 Delta-Mendota Control Structure would be managed using well points for controlled dewatering,
42 while dewatering at the Bethany and Southern Complex pumping plants would be actively managed
43 until structure walls would be connected into underlying clay layers. At all dewatering locations in
44 the Southern Complex, a network of piezometers would be installed to monitor for impacts during

1 construction and allow adaptive management of dewatering practices to maintain local
 2 groundwater conditions. As with the intakes, if needed, Mitigation Measure GW-1: *Maintain*
 3 *Groundwater Supplies in Affected Areas* could be implemented, in which a series of groundwater
 4 recharge and extraction wells could also be installed to allow discharge of captured dewatered
 5 water back into the subsurface in the event that some local external effects due to dewatering are
 6 observed, or for additional groundwater extraction to mitigate for mounded water outside the
 7 construction.

8 Groundwater dewatering events that could temporarily reduce stream gains or increase stream
 9 losses depend on the proximity of the interconnected streams to the construction sites and the rate
 10 and period over which dewatering occurs, as described in the Engineering Project Reports (Delta
 11 Conveyance Design and Construction Authority 2022a, 2022b). For alternatives involving more
 12 intakes (i.e., Alternatives 2a and 4a), the magnitude of dewatering would be higher, but slurry cutoff
 13 walls would be installed around project intake facilities to reduce the amount of groundwater
 14 entering the construction site and the associated need for groundwater dewatering pumping
 15 required for construction. This, in turn, would reduce the potential for impacts on the shallow
 16 aquifer system and on stream gains and/or losses from adjacent streams. As such, the impacts of
 17 these dewatering events on interconnected surface waters would occur during the construction
 18 period and would be short term in nature, and would be minimized through construction practices,
 19 including Mitigation Measure GW-1: *Maintain Groundwater Supplies in Affected Areas*, if needed to
 20 reduce impacts through the recharge of groundwater dewater outside the slurry and/or sheet pile
 21 walls.

22 Operations

23 The cutoff walls described in the *Project Construction* section above should also substantially limit
 24 reduction of external groundwater levels during internal dewatering activities and limit mounding
 25 of water external to the walls during operations when basin levels are higher than the surrounding
 26 groundwater levels.

27 As described in Chapter 3, each alternative would utilize a different number of intakes diverting
 28 surface water at rates up to 1,500 or 3,000 cubic feet per second at each intake. Table 8-2
 29 summarizes the number of intakes and the total amount of water diverted via those intake points in
 30 TAF per year under each project alternative based on the results of the surface water analysis
 31 described in Chapter 6. These diversions may result in changes to the gains or losses from various
 32 reaches of interconnected surface waters in the model domain.

33 **Table 8-2. Number of Intakes and Volume of Surface Water Diverted during Operations by Project**
 34 **Alternative**

Alternative	Number of Intakes	Diversion Capacity (cfs)	Volume of Water Diverted (annual average in TAF)
1	2	6,000	742
2a	3	7,500	775
2b	1	3,000	559
2c	2	4,500	677
3	2	6,000	742
4a	3	7,500	775
4b	1	3,000	559

Alternative	Number of Intakes	Diversion Capacity (cfs)	Volume of Water Diverted (annual average in TAF)
4c	2	4,500	677
5	2	6,000	749

Note: Diversion volumes at the intakes by alternative are from CalSim 3.
TAF = thousand acre-feet.

As simulated in the DeltaGW Model, project operations would result in the diversion of surface water from identified intakes, resulting in a net reduction in surface water flows in the Sacramento River between the intake structures and the Delta. The reduction in streamflow, along with changes in groundwater elevations due to the physical project features, results in differences in stream-aquifer interaction for each project alternative. Stream-aquifer interaction occurs when there is a hydraulic connection between a stream and the underlying aquifer system. Streams can be losing (water going out of stream into the aquifer) or gaining (groundwater coming into stream) at different locations depending on the corresponding hydraulic gradient between the stream and the surrounding groundwater level at those locations. Table 8-3 summarizes the minimum, maximum, and average annual differences between the project alternatives and existing conditions in total stream gains and losses in the entire Sacramento River reach in model subregion 4, with the operating conditions as set forth for each alternative. A negative value in Table 8-3 means that under the alternative, the stream loses more water or gains less water compared to existing conditions. A positive value means that under the alternative, the stream gains more water or loses less water compared to existing conditions. On average, the values are positive, indicating that streams would lose less water or gain more water under the alternative compared to existing conditions. Table 8-4 summarizes the same information for the San Joaquin River reach, and Table 8-5 summarizes the model results for the Suisun Bay reach.

Table 8-3. Annual Minimum, Maximum, and Average Change in Stream Aquifer Interaction relative to Existing Conditions (CEQA Baseline) in the Sacramento River Reach in Model Subregion 4

Alternative	Minimum Difference between Alternative and Existing Conditions	Maximum Difference between Alternative and Existing Conditions	Average Difference between Alternative and Existing Conditions	Exceeds Threshold of Significance (5%)
1	-0.16%	+1.54%	+0.52%	No
2a	+0.04%	+1.69%	+0.62%	No
2b	-0.24%	+0.94%	+0.30%	No
2c	-0.18%	+1.51%	+0.50%	No
3	-0.17%	+1.53%	+0.52%	No
4a	+0.04%	+1.69%	+0.61%	No
4b	-0.24%	+0.94%	+0.29%	No
4c	-0.19%	+1.50%	+0.50%	No
5	-0.17%	+1.53%	+0.52%	No

Note: This table presents the change in stream-aquifer interactions. Negative values mean that under the alternative, the stream loses more water or gains less water when compared to existing conditions. Positive values mean that under the alternative, the stream gains more water or loses less water when compared to existing conditions.

Table 8-4. Annual Minimum, Maximum, and Average Change in Stream Aquifer Interaction relative to Existing Conditions (CEQA Baseline) in the San Joaquin River Reach in Model Subregion 4

Alternative	Minimum Difference between Alternative and Existing Conditions	Maximum Difference between Alternative and Existing Conditions	Average Difference between Alternative and Existing Conditions	Exceeds Threshold of Significance (5%)
1	-0.82%	+0.44%	-0.11%	No
2a	-1.19%	+0.67%	-0.29%	No
2b	-0.54%	+0.58%	-0.03%	No
2c	-0.58%	+0.45%	-0.09%	No
3	-0.85%	+0.40%	-0.11%	No
4a	-1.21%	+0.87%	-0.28%	No
4b	-0.63%	+0.61%	-0.02%	No
4c	-0.77%	+0.42%	-0.08%	No
5	-0.84%	+0.47%	-0.11%	No

Note: This table presents the change in stream-aquifer interactions. Negative values mean that under the alternative, the stream loses more water or gains less water when compared to existing conditions. Positive values mean that under the alternative, the stream gains more water or loses less water when compared to existing conditions.

Table 8-5. Annual Minimum, Maximum, and Average Change in Stream-Aquifer Interaction relative to Existing Conditions (CEQA Baseline) in Suisun Bay reach in Model Subregion 1

Alternative	Minimum Difference between Alternative and Existing Conditions	Maximum Difference between Alternative and Existing Conditions	Average Difference between Alternative and Existing Conditions	Exceeds Threshold of Significance (5%)
1	-0.64%	+1.05%	+0.21%	No
2a	-0.64%	+1.27%	+0.24%	No
2b	-0.64%	+1.14%	+0.15%	No
2c	-0.67%	+1.11%	+0.17%	No
3	-0.64%	+1.05%	+0.21%	No
4a	-0.64%	+1.27%	+0.24%	No
4b	-0.64%	+1.14%	+0.15%	No
4c	-0.67%	+1.11%	+0.17%	No
5	-0.57%	+1.05%	+0.22%	No

Note: This table presents the change in stream-aquifer interactions. Negative values mean that under the alternative, the stream loses more water or gains less water when compared to existing conditions. Positive values mean that under the alternative, the stream gains more water or loses less water when compared to existing conditions.

Under all project alternatives, annual changes in simulated stream gains or losses in the Delta region as a percentage of total annual stream-aquifer interaction from the corresponding stream reach are less than 5%.

1 **CEQA Conclusion—All Project Alternatives**

2 Impacts on groundwater elevations from dewatering as part of project construction would be
3 reduced through the use slurry cutoff walls and/or sheet piles, minimizing changes in groundwater
4 elevations in the shallow aquifer system and interconnected surface water system gains and/or
5 losses resulting from dewatering activities during construction. Maintaining the water conveyance
6 facilities may also require dewatering. During annual removal of sediment, the sedimentation basin
7 at the intake structure would not need to be drained. Water removed during the infrequent
8 dewatering for structural repairs to the sedimentation basins would probably occur for a brief time
9 and would not affect surrounding groundwater levels enough to cause substantial changes in stream
10 aquifer interactions because, similar to the construction phase, dewatered water would be
11 discharged back into the groundwater aquifer in the event of a significant drop in levels outside the
12 cutoff walls. Also, dewatering during operations and maintenance would occur very infrequently
13 (likely decades between events). However, impacts on groundwater conditions and interconnected
14 surface waters could vary by location and at a small-scale during construction. Mitigation Measure
15 *GW-1: Maintain Groundwater Supplies in Affected Areas* would reduce impacts during construction
16 and O&M to less than significant, even for those alternatives that have the highest number of intakes
17 with larger construction footprints.

18 Minimum changes in interconnected Sacramento River flows resulting from project operations
19 range from -0.24% to +0.04% of annual stream-aquifer interaction, while maximum changes in
20 interconnected flow range from +0.94% to +1.69% of annual stream-aquifer interaction. On an
21 average annual basis, differences in Sacramento River flows range from +0.29% to +0.62% of annual
22 stream-aquifer interaction. Therefore, there would be less-than-significant impacts on the overall
23 Sacramento River flows resulting from project operations because the percent differences in
24 Sacramento River flows as simulated between existing conditions and those simulated for each
25 project alternative are less than 5% of the annual stream-aquifer interaction.

26 Minimum changes in interconnected San Joaquin River flows due to project operations range from -
27 0.54% to -1.21% of annual stream-aquifer interaction, while maximum changes in interconnected
28 flow range from +0.40% to +0.87% of annual stream-aquifer interaction. On an average annual
29 basis, differences in San Joaquin River flows range from -0.02% to -0.29% of annual stream-aquifer
30 interaction. Therefore, there would be less-than-significant impacts on the overall San Joaquin River
31 flows resulting from project operations because the percent differences in San Joaquin River flows
32 as simulated between existing conditions and those simulated for each project alternative are less
33 than 5% of the annual stream-aquifer interaction.

34 Minimum changes in interconnected Suisun Bay flows due to project operations range from -0.57%
35 to -0.67% of overall bay flows, while maximum changes in interconnected flow range between
36 +1.05% to +1.27% of overall annual stream-aquifer interaction. On an average annual basis,
37 differences in Suisun Bay flows range from +0.15% to +0.24% of annual stream-aquifer interaction.
38 Therefore, there would be less-than-significant impacts on the overall Suisun Bay flows resulting
39 from project operations because the percent differences in Suisun Bay flows as simulated between
40 existing conditions and those simulated for each project alternative are less than 5% of the annual
41 stream-aquifer interaction.

42 In summary, as changes in the overall flows in interconnected surface water reaches for the
43 Sacramento and San Joaquin Rivers and Suisun Bay resulting from project operations would be
44 minimal, impacts relative to the threshold would be less than significant.

1 **Mitigation Measure GW-1: Maintain Groundwater Supplies in Affected Areas**

2 Prior to construction, the location of existing wells would be determined within the anticipated
3 area of influence of project sites at which dewatering would occur during construction or
4 maintenance. These sites include the north Delta intakes (construction and maintenance), the
5 Southern Forebay Spillway and Outlet Structure (only used during construction dewatering),
6 and the Bethany Complex Surge Basin (only used during construction dewatering). Initially, the
7 area of influence would be considered to be within 0.5 mile of the dewatering areas for each site
8 and will be validated or refined during the design phase.

9 Based on available information, site investigations and desk studies, the location of existing
10 wells, depths of the wells and the depth to groundwater within these wells would be
11 determined. During geotechnical explorations and construction, new monitoring wells would be
12 installed sufficiently close to the groundwater dewatering sites and along the Sacramento River
13 (for the intakes) and Italian Slough (for the Southern Forebay). Existing monitoring wells or new
14 monitoring wells (to be installed as part of field investigations during the design phase) inside
15 and outside the area of influence would also be used. Monitoring would be conducted to assess
16 changes in water levels attributable to dewatering activities and maintenance by comparing
17 changes in groundwater elevations within and outside the dewatering area of influence.
18 Monitoring wells at the intakes would continue to be used as part of a conveyance operations
19 monitoring program.

20 No monitoring would occur near tunnel shaft locations because dewatering would be limited to
21 volume within the constructed tunnel shaft after the shaft has been isolated from the aquifer.

22 Monthly groundwater monitoring would be initiated as soon as access to existing wells was
23 obtained (wherever applicable) and as soon as new monitoring wells were installed. Monitoring
24 would continue through the construction phase for up to 6 months following termination of
25 construction dewatering activities and for at least 5 years after commencement of conveyance
26 operations at the intakes.

27 Monitoring preparation would include:

- 28 ● During the design phase, the locations of existing wells that would require monitoring
29 would be determined. The information would be used to determine the need and location
30 for construction of new monitoring wells. Groundwater levels would be monitored in
31 accessible existing wells. Monitoring of groundwater levels in accessible existing wells
32 would be conducted on a weekly or monthly basis for the durations stated above, as needed.
 - 33 ○ The area of influence of construction dewatering operations and conveyance operations
34 would be refined from the assumed 0.5-mile radius based upon the location of
35 potentially affected existing wells and existing available groundwater and hydrogeologic
36 information.
- 37 ● Additional monitoring wells would be installed at the intakes, Southern Forebay structures,
38 and Bethany Reservoir Surge Basin, as needed, during future geotechnical explorations and
39 the construction phase. Groundwater levels would be monitored in the newly-constructed
40 monitoring wells and existing wells (as noted above). Monitoring of groundwater water
41 levels in new monitoring wells would be conducted on a weekly or monthly basis for the
42 durations stated above, as needed.

- 1 ○ New monitoring wells would be constructed outside the slurry cutoff walls and/or sheet
2 piles, but within the project right-of-way.
- 3 ● All monitoring data would be reported to the public on a monthly basis and in an annual
4 summary report. The monthly reports would contain tabular water level data as well as
5 changes in water levels from the previous months. The annual report would summarize
6 monthly data and show the most recent water level contour map as well as the
7 preconstruction contour map and hydrographs. The final report would include water level
8 contour maps for the area of the groundwater aquifer that is affected by dewatering
9 showing initial, preconstruction water levels, construction phase water levels, post-
10 construction water levels, and annual conveyance operations water levels, as applicable.
- 11 ● The results of preconstruction and construction-related monitoring and geotechnical and
12 hydrogeologic testing during field investigations would be used to determine if
13 supplemental re-injection and/or extraction wells would be needed.

14 During construction or maintenance dewatering, if the results of groundwater monitoring
15 described above indicate that the difference between average groundwater elevation declines in
16 monitoring wells inside the area of influence of dewatering and control (background)
17 monitoring well outside the area of influence is more than 10% of the depth of the shallowest
18 known well inside the area, mitigation of impacts to groundwater supplies would be needed. For
19 wells that may be impacted by groundwater level declines described herein, the following would
20 be implemented:

- 21 ● Reinject groundwater using injection wells; potable supplies would be brought in
22 temporarily while injection wells are constructed and the groundwater basin recharges, if
23 needed.

24 The following additional measures would also be implemented if injection wells are not feasible
25 in an area or not sufficient to offset potential impacts on groundwater levels in the area of
26 influence:

- 27 1. Deepen or modify (e.g., lower pump intakes) wells used for domestic or agricultural
28 purposes; potable supplies would be brought in temporarily while wells are modified, if
29 needed.
- 30 2. Secure a temporary water supply or compensate farmers for production losses due to a
31 reduction in available groundwater supplies.

32 ***Mitigation Impacts***

33 *Compensatory Mitigation*

34 Although the CMP described in Appendix 3F, *Compensatory Mitigation Plan for Special-Status Species*
35 *and Aquatic Resources*, does not act as mitigation for impacts on this resource from project
36 construction or operations, its implementation could result in changes in stream gains or loss
37 impacts.

38 Creation of the wetlands and other habitats on Bouldin Island, at the in I-5 ponds (Ponds 6, 7, and 8),
39 and in the North Delta Arc would result in increased groundwater levels at areas in the vicinity of
40 the new habitats. This, in turn, would affect the local hydraulic gradients resulting in the movement
41 of groundwater from mounds (elevated groundwater levels) under the new ponds and habitats into

1 adjacent stream courses when surface water levels are low. As such, the CMP would benefit
2 interconnected surface waterbodies in the Delta. Therefore, implementation of compensatory
3 mitigation would not change the overall impact conclusion of less than significant.

4 Other Mitigation Measures

5 Other mitigation measures proposed would not have impacts on interconnected stream gains or
6 losses because no mitigation measures would result in the gain or loss of groundwater through
7 activities such as dewatering. Therefore, mitigation measures are unlikely to result in changes in
8 stream gains or losses, and there would be no impact.

9 Overall, changes in stream gains or losses related to compensatory mitigation and implementation
10 of other mitigation measures, combined with project alternatives, would not change the less-than-
11 significant with mitigation impact conclusion.

12 **Impact GW-2: Changes in Groundwater Elevations**

13 Changes in groundwater elevations at and around project facilities are considered to be significant if
14 there is greater than +/-5 feet of change in simulated groundwater elevations more than 5% of the
15 time when compared to simulated groundwater elevations under existing conditions over the
16 duration of the 94-year analysis period from 1922 to 2015.

17 **All Project Alternatives**

18 Changes in groundwater elevations resulting from project construction, including those related to
19 construction-related dewatering, were evaluated qualitatively. Changes in groundwater elevations
20 as a result of project operations were evaluated quantitatively by comparing simulated groundwater
21 levels under existing conditions with those simulated for each project alternative. Groundwater
22 levels were compared at each of the model's 7,977 nodes. The frequency at which the groundwater
23 elevation difference threshold is exceeded is reported for each model node. Detailed simulation
24 results can be found in Appendix 8B.

25 Project Construction

26 Project construction under all project alternatives may result in localized changes to groundwater
27 levels in the immediate area of the constructed facilities. Construction would require some short-
28 term dewatering, as described under Impact GW-1, at facilities such as the Southern Forebay
29 Emergency Spillway, Southern Forebay Outlet Structure, the California Aqueduct Control Structure,
30 and the South Delta Outlet and Control Structure (for Alternatives 1, 2a, 2b, 2c, 3, 4a, 4b, and 4c), and
31 the Delta-Mendota Control Structure (for Alternatives 2a and 4a); and longer-duration dewatering
32 as the intakes are constructed. No dewatering would occur along the tunnel during tunnel boring,
33 and limited removal of groundwater would occur as a result of tunnel shaft construction.

34 During construction dewatering of the intakes, groundwater levels would be lowered to about -20
35 feet mean sea level (MSL) via pumping and maintained at those levels during construction of
36 facilities in the deeper excavations, such as the sedimentation basin. Slurry cutoff walls would be
37 installed around project intake to reduce the amount of dewatering pumping required for
38 construction.

39 Slurry cutoff walls would also be installed as part of the tunnel launch shaft construction. Once the
40 slurry cutoff walls were in place, the tunnel launch shaft would be excavated and an approximately

1 30-foot-thick concrete base slab would be placed at the bottom of the shaft. The concrete plugs
2 constructed in the bottom of the shafts would isolate the shafts from the adjacent groundwater
3 basins prior to removing the isolated water from the shaft.

4 The highest amount of dewatering pumping would occur at the intakes with continuous
5 groundwater pumping at rates ranging from 100 gpm to 2,000 gpm, as described in the the
6 Engineering Project Reports (Delta Conveyance Design and Construction Authority 2022a, 2022b).
7 That dewatering activity could result in short-term lowered groundwater levels locally and a short-
8 term loss of groundwater in storage. However, as previously described under Impact GW-1,
9 monitoring of potential groundwater level impacts during construction would occur for these
10 dewatering activities. If required to mitigate potential impacts, Mitigation Measure GW-1: *Maintain*
11 *Groundwater Supplies in Affected Areas*, would be implemented in which a series of groundwater
12 recharge and extraction wells would be installed around the external perimeter of each intake cutoff
13 wall system to allow discharge of captured dewatered water back into the subsurface on the
14 external side of the deep cutoff walls in the event that local external effects due to dewatering
15 exceed average seasonal variations. Conversely, these wells could be used to extract mounded water
16 for return to the sedimentation basins if needed to maintain local groundwater levels.

17 Sheet piles would be used during construction at the Southern Forebay Emergency Spillway and
18 Southern Forebay Outlet. Similar to the slurry cutoff walls at the intakes, the sheet pile walls would
19 limit impacts on groundwater levels from dewatering, and as with the intake facilities, piezometers
20 would be installed and used to monitor for impacts during construction and for adaptive
21 management during dewatering activities. If local groundwater level variations exceed average
22 season averages, Mitigation Measure GW-1: *Maintain Groundwater Supplies in Affected Areas*, would
23 be implemented in which a series of groundwater recharge and extraction wells would also be
24 installed to allow discharge of captured dewatered water back into the subsurface in the event that
25 local external effects due to dewatering exceed average seasonal variations, or for additional
26 groundwater extraction to mitigate for mounded water outside the construction.

27 Dewatering at the Outlet and Control Structures west of Byron Highway, and the Delta-Mendota
28 Control Structure would be managed using well points for controlled dewatering, while dewatering
29 at the Bethany and Southern Complex pumping plants would be actively managed until structure
30 walls are keyed into underlying clay layers. At all dewatering locations in the Southern Complex, a
31 network of piezometers would be installed for monitoring for impacts during construction to allow
32 management of dewatering practices to maintain average local seasonal groundwater conditions, as
33 needed under Mitigation Measure GW-1.

34 Operations

35 Surface water diverted from the project's north Delta intakes would result in a reduction in surface
36 water flows, which, in turn, may reduce recharge to the underlying groundwater basins resulting in
37 changes to groundwater elevations. Additionally, the physical presence of the project facilities may
38 act as no-flow barriers to subsurface groundwater flow and could result in changes to groundwater
39 flow direction and/or the reflection of pumping depressions, resulting in increases or decreases in
40 groundwater elevations.

41 Shallow (i.e., upper 200 feet) groundwater zones are those that could be affected by the presence of
42 project infrastructure and by diversion of surface water at the intakes. The tunnel outside diameter
43 would range from 28 to 44 feet depending upon the project design capacity. The top of the tunnel
44 would generally be located between 100 and 120 feet bgs; and the bottom of the tunnel would

generally be located between 140 and 160 feet bgs. This depth correlates to the upper three layers of the DeltaGW Model. In the model, layer 1 extends from the ground surface to a depth of 65 feet bgs. Layer 2 extends from 65 feet bgs to 115 bgs, and layer 3 extends from 115 bgs to 165 feet bgs. Simulated groundwater changes in these model layers were used to evaluate potential impacts from operations under the nine project alternatives.

Table 8-6 presents the time frequency of number of model nodes exceeding +/-5 feet change in groundwater elevations for each project alternative relative to existing conditions. The impacts of project operations on groundwater elevations in the model area under all project alternatives are considered to be less than significant because zero model nodes exceed the +/- 5-foot difference threshold more than 5% of the time (56 months) of the 94-year (1,128 months) model simulation period in a monthly time step.

Table 8-6. Number of Model Nodes Exceeding Various Difference Thresholds in Groundwater Elevations relative to Existing Conditions in more than 5% of the Total Simulation Months

Alternative	+/- 1 ft to +/- 2 ft	+/- 2 ft to +/- 3 ft	+/- 3 ft to +/- 4 ft	+/- 4 ft to +/- 5 ft	> +/- 5 ft	Exceeds Threshold of Significance (> +/- 5 ft more than 5% of simulation months)
1	22	2	0	0	0	No
2a	65	2	1	1	0	No
2b	10	0	0	0	0	No
2c	21	1	0	0	0	No
3	24	2	0	0	0	No
4a	69	2	1	1	0	No
4b	12	0	0	0	0	No
4c	23	1	0	0	0	No
5	26	4	1	0	0	No

Note: Analysis is conducted over a 94-year simulation period or 1,128 months. Five percent of months equals 56 months. Total number of nodes in the model = 7,977. Each node has an average effective area of 0.6 square mile; differences evaluated using an average of the simulated groundwater elevations across the top three layers of the model.

Dewatering associated with project maintenance would occur periodically at the intakes and only in rare cases when repairs were needed. During annual removal of sediment, the sedimentation basin at the intake structure would not need to be drained. Water removed during the infrequent dewatering for structural repairs to the sedimentation basins is expected to occur for a brief time and the flows would be tested prior to discharge. Dewatering associated with project maintenance would be managed similarly to dewatering operations during construction.

CEQA Conclusion—All Project Alternatives

Impacts on groundwater elevations from dewatering as part of project construction and/or maintenance would be lessened through the use of slurry cutoff walls as part of project construction. In addition, localized impacts on existing groundwater wells during project construction would be avoided by monitoring groundwater elevations adjacent to construction dewatering locations during project construction. This monitoring process is described in the Engineering Project Reports (Delta Conveyance Design and Construction Authority 2022a, 2022b) and, if needed,

1 Mitigation Measure GW-1: *Maintain Groundwater Supplies in Affected Areas*, would be implemented
2 to allow discharge of captured dewatered water back into the subsurface on the external side of the
3 construction in the event that some local external effects beyond average seasonal variation due to
4 dewatering are observed, or for additional groundwater extraction to address mounded water
5 outside the construction. Potential groundwater level impacts are expected to be short-term and
6 localized in nature, but local conditions can vary so impacts may have the potential to occur. In
7 addition to the steps described in the Engineering Project Reports, Mitigation Measure GW-1:
8 *Maintain Groundwater Supplies in Affected Areas* is available to further address construction-related
9 effects on groundwater.

10 Additionally, as simulated in the DeltaGW Model, no model nodes exceeded the +/- 5-foot change in
11 groundwater elevations in more than 5% of the simulated months resulting from simulated project
12 operations for each alternative. As such, the impact is less than significant and Mitigation Measure
13 GW-1 is available to further ensure impacts on local groundwater supplies is avoided during the
14 construction and operation phases of DCP.

15 **Mitigation Measure GW-1: Maintain Groundwater Supplies in Affected Areas**

16 See description of Mitigation Measure GW-1 under Impact GW-1.

17 ***Mitigation Impacts***

18 *Compensatory Mitigation*

19 Although the CMP described in Appendix 3F does not act as mitigation for impacts on this resource
20 from project construction or operations, its implementation could result in changes in groundwater
21 elevation impacts.

22 Creation of the wetlands and other habitats on Bouldin Island, at the I-5 ponds (Ponds 6, 7, and 8), in
23 the North Delta Arc would result in increased groundwater levels at areas in the vicinity of the new
24 habitats, thereby lessening potential drops in groundwater elevations during project construction
25 and operations. The CMP would have a positive impact on groundwater elevations. Therefore,
26 implementation of compensatory mitigation would not change the overall impact conclusion of less
27 than significant.

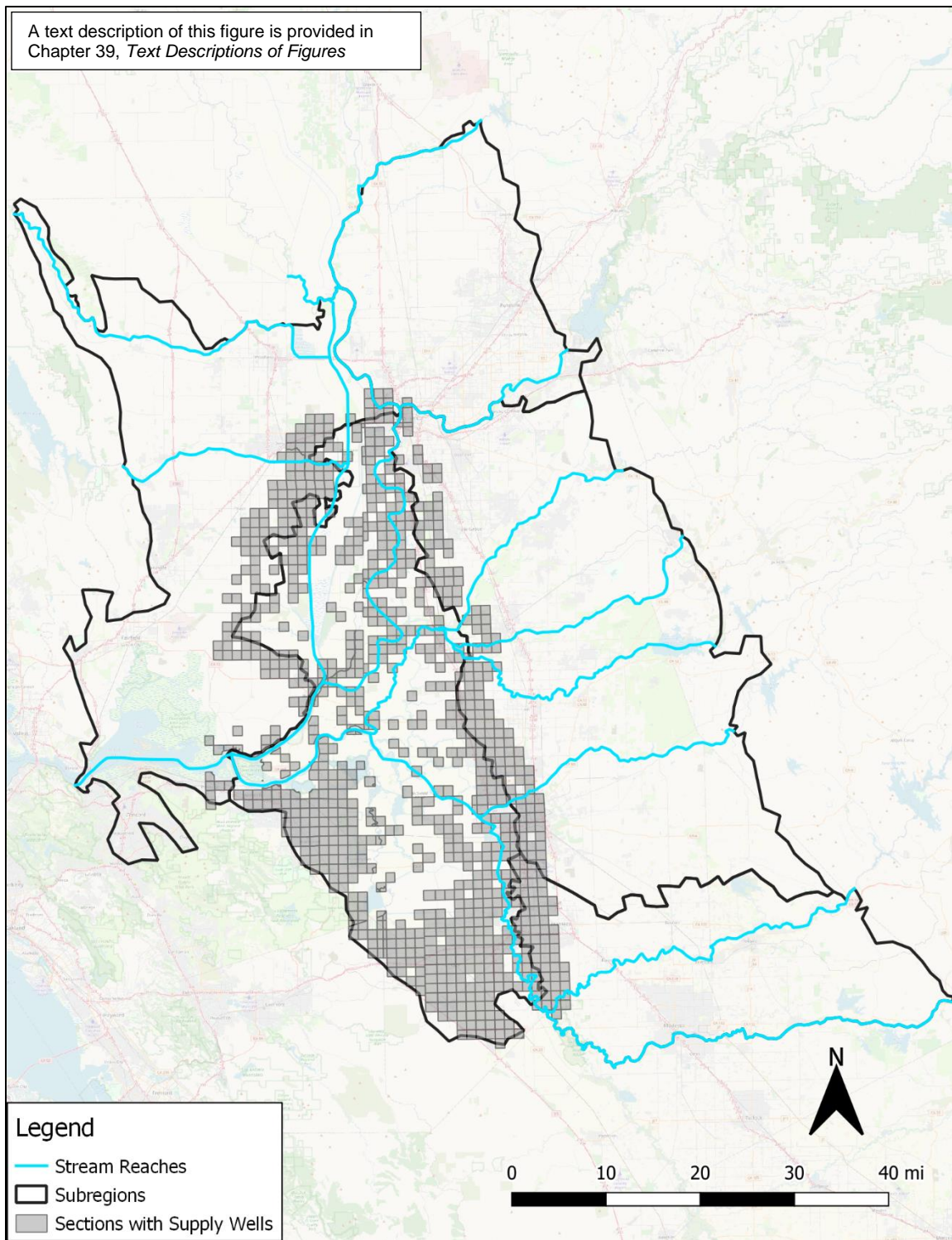
28 *Other Mitigation Measures*

29 Other mitigation measures proposed would not have impacts on groundwater elevations because no
30 mitigation measures would involve activities such as dewatering. Impacts on groundwater
31 elevations from dewatering as part of project construction and/or maintenance would be lessened
32 through the use of slurry cutoff walls and/or sheet piles as part of project construction. Therefore,
33 mitigation measures are unlikely to result in changes in groundwater elevations, and there would be
34 no impact.

35 Overall, changes in groundwater elevations related to compensatory mitigation and other mitigation
36 measures, combined with project alternatives, would not change the less-than-significant with
37 mitigation impact conclusion.

1 Impact GW-3: Reduction in Groundwater Levels Affecting Supply Wells

2 Reductions in groundwater levels are considered significant when they result in declines that
3 exceed 20 feet at any supply well in the Delta region. Project operations were simulated in the
4 DeltaGW Model to identify when declines in groundwater elevations of 20 feet or more relative to
5 the existing conditions (CEQA baseline) elevations may occur at any supply well within 3 miles of
6 the statutory Delta boundary. A total of 5,244 production wells across 918 PLSS sections were
7 identified from DWR's OSWCR database for evaluation. The exact locations of the wells are not
8 known, only the PLSS section number of wells are known. As a result, DeltaGW Model results were
9 evaluated at the centroid of each PLSS section to determine the total number of supply wells that
10 could be affected by project operations due a decline in groundwater elevations when comparing
11 the simulated groundwater levels of alternatives with the existing conditions (CEQA baseline).
12 Figure 8-6 shows the location of the 918 PLSS sections containing supply wells within 3 miles of the
13 statutory Delta boundary as simulated in the DeltaGW Model.



1
2

Figure 8-6. PLSS Sections with Supply Wells Within 3 Miles of the Delta Region

1 ***All Project Alternatives***

2 Changes in groundwater elevations resulting from project construction, including those related to
3 construction-related dewatering, and the potential to affect location supply wells were evaluated
4 qualitatively. Changes in groundwater elevations as a result of project operations were evaluated by
5 comparing simulated groundwater levels under existing conditions at identified supply well
6 locations with those simulated for each project alternative. Detailed simulation results can be found
7 in Appendix 8B.

8 ***Project Construction***

9 Project construction under all project alternatives may result in changes to groundwater levels in
10 the immediate area of the constructed facilities with long-duration groundwater dewatering, such as
11 at the intake locations. Construction would require some short-term dewatering at the tunnel shafts
12 (few weeks at each shaft) and for a few months at the Southern Forebay Emergency Spillway, the
13 Southern Forebay Outlet Structure, the California Aqueduct Control Structure, and the South Delta
14 Outlet and Control Structure (for Alternatives 1, 2a, 2b, 2c, 3, 4a, 4b, and 4c); the Delta-Mendota
15 Control Structure (for Alternatives 2a and 4a) during construction; and longer-duration dewatering
16 as the intakes are constructed.

17 As previously noted, during construction dewatering of the intakes, groundwater levels would be
18 lowered to about -20 feet MSL via pumping and maintained at those levels during construction of
19 facilities in the deeper excavations, such as the sedimentation basin. Slurry cutoff walls and/or sheet
20 pile walls would be installed around project intake and tunnel shaft facilities to reduce the amount
21 of dewatering pumping required for construction. Concrete plugs would be constructed in the
22 bottom of the shafts to isolate the shafts from the adjacent groundwater basins prior to removing
23 the isolated water from the shaft. The highest amount of dewatering pumping would occur at the
24 intakes with continuous groundwater pumping at rates ranging from 100 gpm to 2,000 gpm, as
25 described in the Engineering Project Reports. This dewatering could result in short-term lowered
26 groundwater levels locally at neighboring supply wells and a short-term loss of groundwater in
27 storage (Delta Conveyance Design and Construction Authority 2022a, 2022b). However, as
28 previously described under Impact GW-1, piezometers would be installed outside the slurry wall
29 and/or sheet pile walls to allow monitoring of potential groundwater level impacts affecting
30 neighboring supply wells during construction for adaptive management of dewatering activities. If
31 required to mitigate potential impacts, Mitigation Measure GW-1: *Maintain Groundwater Supplies in*
32 *Affected Areas*, would be implemented in which a series of groundwater recharge and extraction
33 wells would be installed around the external perimeter of each intake cutoff wall system to allow
34 discharge of captured dewatered water back into the subsurface in the event that local external
35 effects on neighboring supply wells due to dewatering beyond average seasonal variation are
36 observed. Conversely, these wells could be used to extract mounded water for return to the
37 sedimentation basins if needed to maintain local groundwater levels.

38 Sheet piles would be used during construction at the Southern Forebay Emergency Spillway and
39 Southern Forebay Outlet. Similar to the cutoff walls at the intakes, the sheet pile walls would limit
40 impacts on groundwater levels from dewatering, and as with the intake facilities, piezometers would
41 be installed and used to monitor for impacts during construction and for adaptive management
42 during dewatering activities. If needed, Mitigation Measure GW-1: *Maintain Groundwater Supplies in*
43 *Affected Areas*, would be implemented in which a series of groundwater recharge and extraction
44 wells would also be installed to allow discharge of captured dewatered water back into the
45 subsurface in the event that local external effects due to dewatering beyond average seasonal

1 variation are observed, or for additional groundwater extraction to mitigate for mounded water
2 outside the construction.

3 Dewatering at the Outlet and Control Structures west of Byron Highway, and the Delta-Mendota
4 Control Structure would be managed using well points for controlled dewatering, while dewatering
5 at the Bethany and Southern Complex pumping plants would be actively managed until structure
6 walls are keyed into underlying clay layers. At all dewatering locations in the Southern Complex, a
7 network of piezometers would be installed for monitoring for impacts during construction to allow
8 management of dewatering practices to maintain local groundwater conditions within average
9 seasonal variation limits.

10 Operations

11 Project operations have the potential to influence groundwater elevations. Surface water diverted at
12 the project's intakes may result in a reduction in surface water flows which, in turn, may reduce
13 recharge to the underlying groundwater basins resulting in changes to groundwater elevations.
14 Additionally, the physical presence of the project facilities may act as no-flow barriers to subsurface
15 groundwater flow and could result in changes to groundwater flow direction and/or the reflection
16 of pumping depressions, resulting in increases or decreases in groundwater elevations.

17 Table 8-7 presents the number of supply wells with groundwater elevations declines relative to
18 existing conditions from operations of each project alternative. Some of the wells evaluated may fall
19 within the project construction boundaries. The OSWCR database used for the analysis does not
20 include exact coordinates for each well so specific wells could not be excluded from the analysis,
21 such as wells that would be within the project construction boundaries. The impacts of project
22 operations on groundwater elevations in the underlying subbasin under all project alternatives are
23 considered to be less than significant because there are no supply wells exceeding the 20 feet or
24 more of groundwater elevation change threshold, and the maximum number of supply wells
25 experiencing a 2-foot change in groundwater elevation as a result of project operations (well within
26 typical background water level fluctuations) is only 12, representing less than 1% of all supply wells
27 within 3 miles of the statutory Delta boundary.

28 **Table 8-7. Number of Supply Wells with Decline in Groundwater Elevations Relative to Existing**
29 **Conditions**

Alternative	1 ft to 2 ft Decline	2 ft to 3 ft Decline	3 ft to 4 ft Decline	4 ft to 5 ft Decline	5 ft to 10 ft Decline	10 ft to 15 ft Decline	15 ft to 20 ft Decline	> 20 ft Decline	Exceeds Threshold of Significance (>20 ft Decline)
1	55	12	0	0	0	0	0	0	No
2a	75	11	0	0	0	0	0	0	No
2b	40	2	0	0	0	0	0	0	No
2c	54	12	0	0	0	0	0	0	No
3	55	12	0	0	0	0	0	0	No
4a	75	11	0	0	0	0	0	0	No
4b	40	2	0	0	0	0	0	0	No
4c	54	12	0	0	0	0	0	0	No
5	52	12	0	0	0	0	0	0	No

30 Note: This table evaluates the changes in groundwater elevations at supply wells in the region based on the PLSS section
31 they reside. Some wells may fall within project construction boundaries. Number of wells shown in the table are based on
32 the number wells within the PLSS sections that fall within each range of groundwater elevation declines.

1 ***CEQA Conclusion—All Project Alternatives***

2 Under all project alternatives, groundwater dewatering would occur during construction of the
3 intakes (sedimentation basins) and the Southern Complex. Impacts on groundwater elevations from
4 dewatering as part of project construction have the potential to significantly affect local
5 groundwater elevations and, in turn, the use of nearby supply wells. These impacts would be
6 reduced through the use of slurry and/or sheet pile cutoff walls (at the intake and tunnel shafts) and
7 sheet piles (at the Southern Forebay Spillway and Outlet) to separate the dewatered area from the
8 surrounding groundwater basin. Areas adjacent to construction dewatering locations would be
9 monitored for potential impacts on groundwater levels and associated operational impacts on wells
10 in the area of effect (Delta Conveyance Design and Construction Authority 2022a) as described in
11 Chapter 3, *Description of the Proposed Project and Alternatives*. Should impacts on surrounding
12 groundwater levels, and therefore potentially on nearby supply wells, be observed beyond average
13 seasonal variation, dewatering operations would be managed, including the use of Mitigation
14 Measure GW-1: *Maintain Groundwater Supplies in Affected Areas*, if required. With this mitigation
15 measure, impacts would be lessened through the combined use of slurry cutoff walls/sheet piles and
16 recharge wells outside the dewatering area to generally “circulate” shallow groundwater, thereby
17 reducing significant changes in groundwater elevations, and associated impacts on supply wells,
18 resulting from dewatering activities.

19 Drops in simulated groundwater elevations as a result of project operations would not exceed 20
20 feet at any identified supply well within the DeltaGW Model domain. Additionally, only roughly 2%
21 of identified supply wells within the model domain would experience groundwater elevation
22 declines between 5 and 10 feet resulting from simulated project operations for each alternative
23 (within the range typically seen as a result of hydrologic fluctuations). As such, the impact is less
24 than significant for operations for all project alternatives relative to reductions in groundwater
25 elevations affecting supply wells.

26 **Mitigation Measure GW-1: Maintain Groundwater Supplies in Affected Areas**

27 See description of Mitigation Measure GW-1 under Impact GW-1.

28 ***Mitigation Impacts***

29 *Compensatory Mitigation*

30 Although the CMP described in Appendix 3F does not act as mitigation for impacts on this resource
31 from project construction or operations, its implementation could result in reduction in
32 groundwater level impacts.

33 Use of surface water for creation of the wetlands and other habitats on Bouldin Island, at the I-5
34 ponds (Ponds 6, 7, and 8), and in the North Delta Arc would result in increased groundwater levels
35 at areas in the vicinity of the new habitats. This, in turn, would minimize impacts on nearby supply
36 wells stemming from decreases in groundwater elevations resulting from project construction and
37 operations. Thus, the CMP would have a positive impact on groundwater elevations. Therefore,
38 implementation of compensatory mitigation would not change the overall impact conclusion of less
39 than significant.

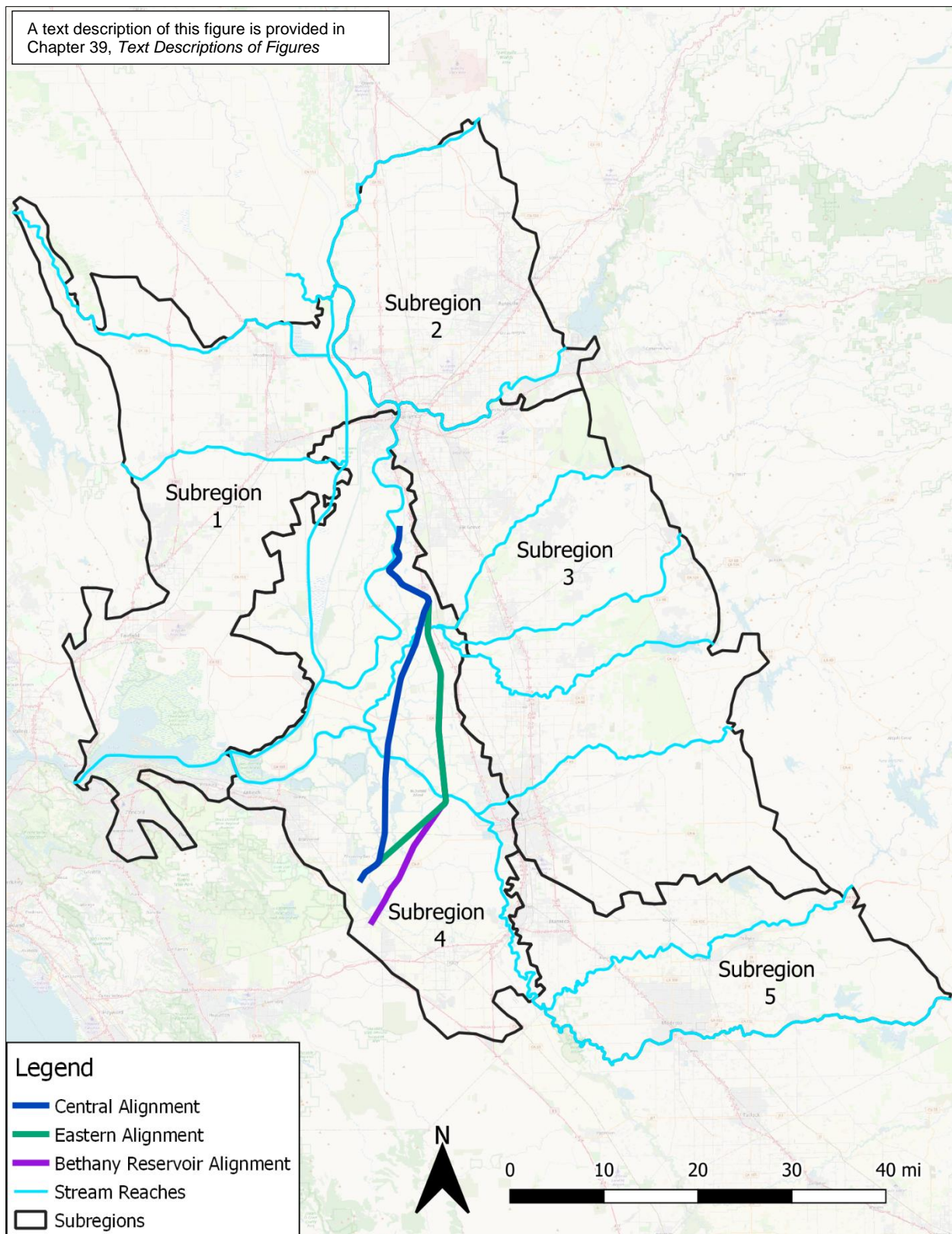
1 *Other Mitigation Measures*

2 Some mitigation measures would involve providing new water wells or relocating and/or replacing
3 wells, pipes, power lines, drainage systems, and other infrastructure that would have the potential
4 to result in a reduction in groundwater levels. The mitigation measure with potential to result in a
5 reduction in groundwater levels affecting supply wells is Mitigation Measure AG-2: *Replacement or*
6 *Relocation of Affected Infrastructure Supporting Agricultural Properties*. Temporary reductions in
7 groundwater levels resulting from mitigation measures would be similar to construction effects of
8 the project alternatives in certain construction areas and would contribute to groundwater level
9 impacts of the project alternatives. Mitigation measures involving short-term groundwater
10 dewatering may result in temporary changes to groundwater levels. The impacts of operating
11 relocated and/or replaced wells on groundwater elevations in the underlying subbasin are not
12 substantial because there are no supply wells exceeding the 20 feet or more of groundwater
13 elevation change threshold. In addition, groundwater elevations would be tracked through
14 groundwater monitoring programs to prevent changes in groundwater levels. Therefore, other
15 mitigation measures are unlikely to reduce groundwater levels affecting supply wells and the impact
16 of groundwater levels would not be substantial.

17 Overall, the impact of reduced groundwater levels from construction of compensatory mitigation
18 and implementation of other mitigation measures, combined with project alternatives, would not
19 change the less-than-significant with mitigation impact conclusion.

20 **Impact GW-4: Changes to Long-Term Change in Groundwater Storage**

21 Changes in groundwater storage are considered to be significant when there is more than a 5%
22 decrease in the change in long-term change in aquifer storage in the DeltaGW Model subregion 4
23 (the model subregion containing the project footprint) relative to existing conditions. DeltaGW
24 Model subregion 4 overlies the Tracy, East Contra Costa, Solano, Yolo, Eastern San Joaquin, South
25 American, and Cosumnes groundwater subbasins, of which the Eastern San Joaquin Basin has been
26 designated by DWR as being in critically overdrafted condition. Figure 8-7 shows the location of
27 project infrastructure in the DeltaGW Model subregion 4.



1
2

Figure 8-7. Location of Project Infrastructure in the DeltaGW Model

1 ***All Project Alternatives***

2 Project construction–related impacts on the long-term change in groundwater in storage were
3 evaluated qualitatively. Project operations–related changes in long-term change in groundwater
4 storage in the groundwater basins underlying project facilities were evaluated quantitatively using
5 the DeltaGW Model by comparing the long-term change in groundwater in storage over the model
6 period as determined under existing conditions with that simulated for each project alternative.
7 Detailed model results can be found in Appendix 8B.

8 ***Project Construction***

9 Project construction under all project alternatives may result in changes to the volume of
10 groundwater in the immediate area of the constructed facilities. Construction would require some
11 short-term dewatering that may result in the reduction of groundwater in storage in the area of
12 those facilities. Slurry cutoff walls or sheet piles would be constructed around facilities requiring
13 dewatering (such as the intakes, tunnel shafts, and Southern Forebay Spillway and Outlet Structure)
14 to reduce impacts of the dewatering pumping. However, reductions in the volume of groundwater in
15 storage as a result of project construction where dewatering would occur for several years, though
16 anticipated to be localized and short-term in nature, may be considered significant without
17 mitigation. Mitigation Measure GW-1: *Maintain Groundwater Supplies in Affected Areas*, would
18 further address these impacts through the recharge of groundwater outside the slurry walls/sheet
19 piles as needed. Groundwater dewatering at the tunnel shaft locations would occur for only a few
20 weeks and be limited to the volume of water inside the shaft after the shaft is constructed and sealed
21 from the adjacent groundwater. Groundwater dewatering at the Southern Forebay Emergency
22 Spillway would occur for a few months and be adjacent to Italian Slough; but dewatering at this
23 location would be managed using sheet piles. Additionally, dewatering would occur at the Southern
24 Forebay Outlet Structure, the California Aqueduct Control Structure, and the South Delta Outlet and
25 Control Structure (for Alternatives 1, 2a, 2b, 2c, 3, 4a, 4b, and 4c), and the Delta-Mendota Control
26 Structure (for Alternatives 2a and 4a); however, at these locations, construction dewatering would
27 be local, or in the case of the pumping plants, the structural foundation would be keyed into
28 underlying clay layers. Construction activities with implementation of Mitigation Measure GW-1 are
29 not anticipated to result in significant impacts on groundwater in storage.

30 ***Operations***

31 Surface water diverted at the project intakes would result in a reduction in surface water flows
32 which, in turn, may reduce recharge to the underlying groundwater basins, resulting in changes to
33 the volume of groundwater in storage at any one time. For each project alternative, Table 8-8
34 presents the long-term change in groundwater storage in AF, the difference in long-term
35 groundwater storage relative to existing conditions (also in AF), and the percent difference in long-
36 term groundwater storage relative to existing conditions as a result of project operations. Under
37 existing conditions, the long-term change in groundwater storage declines 900,666 AF over the 94-
38 year simulation period. The total area of DeltaGW subregion 4 is 718,470 acres. The relative change
39 in storage in terms of AF per acre is also provided in Table 8-8 for additional context. Under all
40 project alternatives, the region would see an increase in groundwater storage due to increased
41 surface water supplies, as simulated in the surface water analysis. The increase in surface water
42 supply reduces groundwater use and thus reduces the decline in groundwater storage.

1 **Table 8-8. Long-Term Change in Groundwater Storage in Acre-Feet and Change Relative to Existing**
 2 **(CEQA Baseline) Conditions**

Alternative	Long-Term Change in Groundwater Storage (AF)	Increase (+) / Decrease (-) relative to Existing Conditions (AF)	Increase (+) / Decrease (-) relative to Existing Conditions (AF/Acre)	Percent difference relative to Existing Conditions	Exceeds Threshold of Significance (More than 5% Decrease)
Existing Conditions (CEQA Baseline)	-900,666	N/A	N/A	N/A	N/A
1	-888,318	+12,348	+0.017	+1.37%	No
2a	-879,382	+21,285	+0.030	+2.36%	No
2b	-893,318	+7,349	+0.010	+0.82%	No
2c	-889,901	+10,765	+0.015	+1.20%	No
3	-888,860	+11,807	+0.016	+1.31%	No
4a	-879,757	+20,909	+0.029	+2.32%	No
4b	-893,771	+6,895	+0.010	+0.77%	No
4c	-890,442	+10,224	+0.014	+1.14%	No
5	-883,656	+17,010	+0.024	+1.89%	No

3 Note: Negative values indicate a reduction in change in storage.
 4

5 ***CEQA Conclusion—All Project Alternatives***

6 Reductions of groundwater in storage resulting from dewatering activities as part of project
 7 construction and/or maintenance would be lessened through the use of slurry cutoff walls and sheet
 8 piles during construction. Areas adjacent to construction dewatering locations would be monitored
 9 for potential impacts on groundwater levels, which would be mitigated as needed under Mitigation
 10 Measure GW-1: *Maintain Groundwater Supplies in Affected Areas*. Changes in groundwater levels and
 11 the area over which those changes occur can be used to calculate potential changes in groundwater
 12 in storage. The spacing, depth, and location of recharge wells and monitoring piezometers, as well as
 13 thresholds for target external groundwater levels, would be determined after further site-specific
 14 investigation, testing, and analysis during future design phases.

15 Additionally, the percent change of volume of groundwater in storage during operations, as
 16 calculated by DeltaGW Model simulations as compared to existing conditions, was less than 5%
 17 under all project alternatives. As such, the impact is less than significant for all project alternatives
 18 relative to changes in the volume of groundwater in storage for construction and operations. In
 19 addition, Mitigation Measure GW-1 is available to further ensure impacts on local groundwater
 20 supplies are avoided during operation of the DCP.

21 **Mitigation Measure GW-1: Maintain Groundwater Supplies in Affected Areas**

22 See description of Mitigation Measure GW-1 under Impact GW-1.

1 ***Mitigation Impacts***

2 *Compensatory Mitigation*

3 Although the CMP described in Appendix 3F does not act as mitigation for impacts on this resource
4 from project construction or operations, its implementation could result in groundwater storage
5 impacts.

6 Creation of the wetlands and other habitats on Bouldin Island, at the I-5 ponds (Ponds 6, 7, and 8),
7 and in the North Delta Arc would result in increased recharge to the underlying groundwater basins.
8 This, in turn, would increase the volume of groundwater in storage during project construction and
9 operations. As such, the CMP would have a positive impact on groundwater storage. Therefore,
10 implementation of compensatory mitigation would not change the overall impact conclusion of less
11 than significant.

12 *Other Mitigation Measures*

13 Some mitigation measures would involve providing new water wells or relocating and/or replacing
14 wells, pipes, power lines, drainage systems, and other infrastructure that would have the potential
15 to result in changes to long-term groundwater storage. The mitigation measure with potential to
16 result in changes to long-term groundwater storage is Mitigation Measure AG-2: *Replacement or*
17 *Relocation of Affected Infrastructure Supporting Agricultural Properties*. Temporary changes to long-
18 term groundwater storage resulting from mitigation measures would be similar to construction
19 effects of the project alternatives in certain construction areas and would contribute to groundwater
20 levels impacts of the project alternatives. Mitigation measures involving groundwater dewatering
21 may result in changes to groundwater storage. However, groundwater dewatering associated with
22 mitigation measures would be localized and temporary and would not affect long-term groundwater
23 storage. Therefore, other mitigation measures are unlikely to change long-term groundwater
24 storage and the impact of groundwater storage would not be substantial.

25 Overall, the impact of long-term groundwater storage from construction of compensatory mitigation
26 and implementation of other mitigation measures, combined with project alternatives, would not
27 change the less-than-significant with mitigation impact conclusion.

28 **Impact GW-5: Increases in Groundwater Elevations near Project Intake Facilities Affecting** 29 **Agricultural Drainage**

30 Changes in groundwater elevations at and around project facilities have the potential to affect
31 agricultural drainage operations. Reductions in groundwater elevations through the use of existing
32 agricultural drains help alleviate problems with high groundwater levels affecting the root zones of
33 agricultural operations; therefore, only increases in groundwater elevations are considered to have
34 a negative impact on agricultural operations. Increases in groundwater elevations are considered to
35 be significant relative to impacts on agricultural operations when groundwater level rises cause
36 more than a 10% increase in annual agricultural drainage flows when compared to existing
37 conditions.

38 ***All Project Alternatives***

39 Changes in groundwater elevations, and their resultant changes in agricultural drainage, during
40 project operations were evaluated by comparing simulated groundwater levels and associated

1 volumes of agricultural drainage under existing conditions with those simulated for each project
2 alternative. Detailed simulation results and contour maps showing the changes in groundwater
3 elevations and associated volumes of agricultural drainage can be found in Appendix 8B. Qualitative
4 analyses were performed for project construction.

5 Project Construction

6 Project construction requires the installation of slurry and/or sheet pile cutoff walls around project
7 intake facilities and sheet piles around Southern Forebay facilities to lower groundwater elevations
8 during construction. These cutoff walls also have the potential to act as no-flow boundaries,
9 increasing groundwater levels and potentially increasing root zone inundation. Impacts on
10 groundwater elevations, and on resultant agricultural drainage volumes, as a result of project
11 construction practices are expected to be localized and short-term in nature and are not anticipated
12 to result in significant impacts on groundwater levels. Additionally, as previously discussed,
13 piezometers would be installed outside the slurry walls and sheet piles to allow monitoring of
14 potential groundwater level impacts during construction for adaptive management of construction
15 activities. Further, if needed, Mitigation Measure GW-1: *Maintain Groundwater Supplies in Affected*
16 *Areas*, would be implemented in which a series of groundwater recharge and extraction wells would
17 also be installed within the construction site to allow additional groundwater extraction to mitigate
18 for mounded water outside the slurry walls or sheet piles during project construction, thereby
19 minimizing impacts on agricultural drainage (Delta Conveyance Design and Construction Authority
20 2022a, 2022b).

21 Operations

22 Slurry walls and subsurface project facilities constructed as part of the project have the potential to
23 act as no-flow barriers to groundwater flows and may result in increases in groundwater elevations
24 in the areas immediately near their location. The potential for the increased groundwater elevations
25 to result in increased agricultural drainage was evaluated by comparing the simulated volumes of
26 agricultural drainage occurring in the Delta region under each alternative with that estimated by the
27 model for existing conditions. Increases in agricultural drainage occur as a response to higher
28 groundwater levels. For all alternatives, the maximum groundwater level increase across the Delta
29 region is within 0.5 to 1 foot relative to existing conditions. Increases in agricultural drainage are
30 distributed across the entire Delta region and are not expected to be concentrated in any single area.

31 The results of the CalSim 3 surface water analysis, detailed in Chapter 5, *Surface Water*, and Chapter
32 6, *Water Supply*, show an increase in surface water supplies across the Delta region, which results in
33 decreased groundwater use and a higher water table. Table 8-9 summarizes the volume of
34 agricultural drainage occurring under each alternative simulation in AF, along with the change in
35 drainage relative to existing conditions both as a volume in AF and as a percent change.

1 **Table 8-9. Volume of Agricultural Drainage in Acre-Feet and Percent Change in Agricultural**
 2 **Drainage Relative to Existing Conditions**

Alternative	Volume of Agricultural Drainage (AF)	Increase (+)/Decrease (-) with Respect to Existing Conditions (AF)	Percent Change Relative to Existing Conditions	Exceeds Threshold of Significance (10%)
1	540,746	+320	+0.06%	No
2a	540,954	+528	+0.10%	No
2b	540,915	+489	+0.09%	No
2c	540,652	+226	+0.04%	No
3	540,857	+431	+0.08%	No
4a	541,061	+635	+0.12%	No
4b	541,020	+594	+0.11%	No
4c	540,763	+337	+0.06%	No
5	540,780	+354	+0.07%	No

3

4 **CEQA Conclusion—All Project Alternatives**

5 Impacts resulting in increases in agricultural drainage due to project construction and operations
 6 are considered to be less than significant. At most construction sites, the buried portion of the
 7 facilities or the slurry walls would extend over a very small portion of the site (less than 1% of the
 8 property). At the intakes, the slurry walls would extend over a larger portion of the property;
 9 however, because monitoring would occur during project construction to provide real-time
 10 feedback on groundwater conditions, allowing for modifications to groundwater extractions and
 11 recharge to limit impacts on agricultural operations in the immediate area and aquifer groundwater
 12 elevations (Delta Conveyance Design and Construction Authority 2022a, 2022b). Additionally,
 13 groundwater wells installed through Mitigation Measure GW-1: *Maintain Groundwater Supplies in*
 14 *Affected Areas* would allow additional extraction of groundwater, reducing mounding and associated
 15 impacts relating to project construction.

16 Modeling conducted to simulate project operations shows that changes in agricultural drainage
 17 relative to existing conditions range from a 0.06% increase to a 0.12% increase in agricultural
 18 drainage over the simulated period, all less than the 10% change in agricultural drainage threshold.
 19 The impact on construction and operational-related impacts on agricultural drainage are considered
 20 less than significant. Implementation of Mitigation Measure GW-5: *Increases in Groundwater*
 21 *Elevations Near Project Intake Facilities Affecting Agricultural Drainage*, would further reduce risks
 22 of impacts on agricultural drainage.

23 **Mitigation Measure GW-5: Increases in Groundwater Elevations near Project Intake**
 24 **Facilities Affecting Agricultural Drainage**

25 The groundwater monitoring well system (including existing wells) described under MM GW-1
 26 would be used during construction and maintenance to determine if increases in groundwater
 27 elevations within the area of influence would exceed observed increases outside the area of
 28 influence. If groundwater elevations increase more than 10% inside the area of influence over
 29 conditions outside the area of influence, existing or new dewatering wells (including re-injection

1 wells described for Mitigation Measure GW-1) would be used to extract groundwater and
2 reduce the groundwater elevations to average seasonal elevations.

3 ***Mitigation Impacts***

4 *Compensatory Mitigation*

5 Although the CMP described in Appendix 3F does not act as mitigation for impacts on this resource
6 from project construction or operations, its implementation could result in groundwater elevation
7 impacts.

8 Implementation of the CMP resulting in the creation of the wetlands and other habitats on Bouldin
9 Island, the I-5 ponds (Ponds 6, 7, and 8), and in the North Delta Arc would likely result in increased
10 groundwater levels at areas in the vicinity of the new habitats. These increased groundwater levels,
11 along with increases in groundwater elevations in the study area as a result of project operations,
12 may affect agricultural drainage in the vicinity of wetlands and other habitats sites. Active
13 management of the new wetlands and habitats (i.e., adjusting amounts of applied water) may be
14 able to address localized changes to groundwater levels, further minimizing impacts on agricultural
15 drainage. Given that most of the proposed habitats to be constructed and managed under the CMP
16 are either habitats or seasonal or emergent wetlands, the addition of approximately 10 acres of new
17 depressions (lakes or ponds) in a total area of over 6,000 acres represents an increase of
18 approximately 0.17%; therefore, impacts would not be substantial. Implementation of
19 compensatory mitigation would not change the overall impact conclusion of less than significant.

20 *Other Mitigation Measures*

21 Other mitigation measures proposed would not have impacts on increased groundwater elevations
22 affecting agricultural drainage because no mitigation measures would result in no-flow boundaries
23 or increased groundwater levels and potentially increasing root zone inundation in the area where
24 the alternatives would be constructed or would be operated. Therefore, mitigation measures are
25 unlikely to result in the increase in groundwater elevations affecting agricultural drainage, and there
26 would be no impact.

27 Overall, increases in groundwater elevations affecting agricultural drainage related to compensatory
28 mitigation and implementation of other mitigation measures, combined with project alternatives,
29 would not change the less-than-significant impact conclusion.

30 **Impact GW-6: Damage to Major Conveyance Facilities Resulting from Land Subsidence**

31 Reductions in groundwater elevations at and around project facilities have the potential to cause
32 land subsidence as a result of the removal of groundwater from subsurface formations, resulting in
33 damage to major conveyance facilities. Project construction-related impacts on potential land
34 subsidence were evaluated qualitatively. Also, the evaluation of project operations-related impacts
35 on potential land subsidence was conducted qualitatively because of the lack of availability of land
36 subsidence process model. Instead, declines in groundwater elevations near the major conveyance
37 facilities obtained from the DeltaGW Model results were used to qualitatively infer potential for land
38 subsidence due to project operations.

1 ***All Project Alternatives***

2 As described in Chapter 11, *Soils*, land subsidence in the Delta typically occurs as the result of the
3 oxidation of organic soils. While some of the project facilities would be constructed on soils that are
4 subject to excessive subsidence, geotechnical investigations would be conducted at all facilities to
5 identify the subsidence potential and types of soil avoidance or soil stabilization measures that
6 should be implemented to ensure that the facility settlement is within the design limits or facilities
7 are constructed to withstand subsidence and differential settlement and to conform to applicable
8 state and federal standards. Conformance with these standards would protect the integrity of the
9 project facilities against any subsidence that takes place and would reduce the potential hazard of
10 subsidence or settlement to acceptable levels by avoiding construction directly on or otherwise
11 stabilizing the soil material that is prone to subsidence.

12 Land subsidence south of the Delta (San Joaquin Valley and Tulare Lake region) typically occurs as a
13 result of the removal of groundwater from clay formations, and more significantly, could occur as a
14 result of the removal of groundwater below the Corcoran Clay layer (U.S. Geological Survey
15 2018:47). Decreases in groundwater elevations are indicators of the potential for this impact to
16 occur. As noted in Impact GW-2: *Changes in Groundwater Elevations*, changes in groundwater
17 elevations as simulated during project operations resulted in changes of less than 5 feet across most
18 of the model domain, with dewatering occurring in the upper 165 feet of the groundwater basin.
19 Groundwater elevation changes exceeding 5 feet were infrequent and occurred over a limited area
20 under all alternatives and occurring above significant clay layers and are, therefore, unlikely to
21 result in land subsidence. Detailed simulation results can be found in Appendix 8B.

22 *Project Construction*

23 Project construction under all project alternatives may result in changes to groundwater levels in
24 the immediate area of the constructed facilities. Construction would require some short-term
25 dewatering at the tunnel shafts and Southern Forebay Emergency Spillway, Southern Forebay Outlet
26 Structure, the California Aqueduct Control Structure, and the South Delta Outlet and Control
27 Structure (for Alternatives 1, 2a, 2b, 2c, 3, 4a, 4b, and 4c); the Delta-Mendota Control Structure (for
28 Alternatives 2a and 4a); and for longer duration during construction at the intakes. Decreases in
29 groundwater elevations as a result of project would be localized and short-term in nature, and
30 construction activities would not result in significant impacts on groundwater levels, as described
31 under Impacts GW-2, GW-3, and GW-4. Furthermore, project construction activities would occur at
32 depths above 165 bgs, which is above the Corcoran Clay layer that does not exist in the Delta but
33 may be present in the southeastern edge of the model domain, abutting and into the Eastern San
34 Joaquin and Tracy Subbasins. The depth of Corcoran Clay is approximately 200 feet near the City of
35 Tracy.

36 *Operations*

37 As demonstrated through the simulation of project operations, under all alternatives, groundwater
38 level impacts would occur in the upper three model layers extending from the ground surface to
39 around 165 feet bgs. Furthermore, model results show that groundwater elevation declines of
40 greater than 5 feet occur less than 1% of the time or 1 year of the 94-year simulation period from
41 1922 to 2015. As such, land subsidence from sub-Corcoran Clay pumping would be unlikely to occur
42 as groundwater level impacts would occur in the aquifer above the Corcoran Clay. Land subsidence
43 within the Delta occurs, as previously noted, predominantly as the result of the oxidation of organic

1 soils and would therefore not be influenced by groundwater elevation changes from project
2 operations.

3 ***CEQA Conclusion—All Project Alternatives***

4 Potential subsidence-related impacts resulting from project construction in areas of the Delta with
5 organic soils is addressed in Chapter 11. Construction of some project facilities would require
6 dewatering, which would be reduced through the use of slurry cutoff walls and sheet piles. However,
7 in all cases, dewatering would occur in the upper 165 feet of the aquifer and would, therefore, not
8 result in significant pumping below the Corcoran Clay—a mechanism known to result in inelastic
9 land subsidence south of the Delta (U.S. Geological Survey 2018:47). Therefore, subsidence-related
10 impacts resulting from construction would be less than significant.

11 The likelihood of major project facility operations resulting in groundwater extraction-induced land
12 subsidence would be less than significant because DeltaGW modeling simulations have shown that
13 groundwater elevation changes resulting from project operations would be around 5 feet or less in
14 the upper model layers (extending to 165 feet bgs). Model results show that groundwater elevation
15 declines of greater than 5 feet occur less than 1% of the time or 1 year of the 94-year simulation
16 period from 1922 to 2015. Groundwater extractions from this depth are not sub-Corcoran and
17 therefore would not induce land subsidence and related impacts on facilities resulting from aquifer
18 compaction below the Corcoran Clay.

19 ***Mitigation Impacts***

20 *Compensatory Impacts*

21 Although the CMP described in Appendix 3F does not act as mitigation for impacts on this resource
22 from project construction or operations, its implementation could result in damage to major
23 conveyance facility impacts.

24 Under the CMP, wetlands and other habitats would be created on Bouldin Island, at the I-5 ponds
25 (Ponds 6, 7, and 8), and in the North Delta Arc in the area of the Delta. As described in Chapter 11,
26 *Soils*, dropping land elevations in the Delta is predominantly the result of the oxidation of organic
27 soils, increased groundwater levels resulting from the development of managed wetlands and
28 lakes/ponds may result in increased saturation of soils in the study area, creating anoxic conditions
29 and thereby reducing the potential for additional soil oxidation. Therefore, with implementation of
30 the CMP, there would be little to no impact on land subsidence resulting from groundwater
31 extractions. Implementation of compensatory mitigation would not change the overall impact
32 conclusion of less than significant.

33 *Other Mitigation Measures*

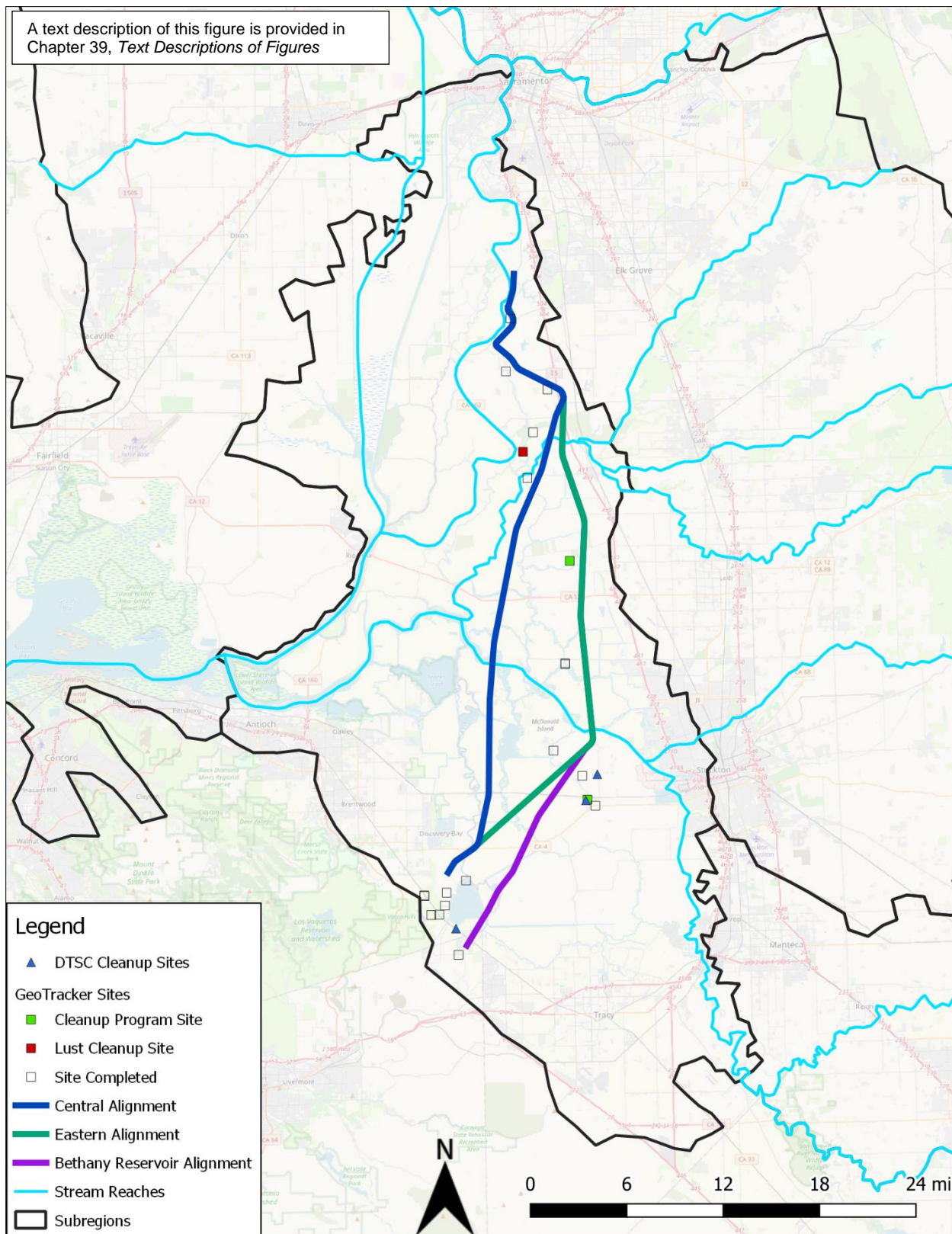
34 Some mitigation measures would involve providing new water wells or relocating and/or replacing
35 wells, pipes, power lines, drainage systems, and other infrastructure that would have the potential
36 to damage major conveyance facilities resulting from land subsidence. The mitigation measure with
37 potential to result in damage to major conveyance facilities resulting from land subsidence is
38 Mitigation Measure AG-2: *Replacement or Relocation of Affected Infrastructure Supporting*
39 *Agricultural Properties*. Temporary land subsidence resulting from mitigation measures would be
40 similar to construction effects of the project alternatives in certain construction areas and would
41 contribute to land subsidence impacts of the project alternatives. Mitigation measures involving

1 localized and short-term groundwater dewatering would not induce land subsidence. Groundwater
2 level management during construction dewatering would minimize the potential for land
3 subsidence and associated damage to major conveyance facilities due to mitigation measures.
4 Therefore, other mitigation measures are unlikely to damage major conveyance facilities resulting
5 from land subsidence and the impact of land subsidence would not be substantial.

6 Overall, the impact of damage to major conveyance facilities resulting from land subsidence from
7 construction of compensatory mitigation and implementation of other mitigation measures,
8 combined with project alternatives, would not change the less-than-significant impact conclusion.

9 **Impact GW-7: Degradation of Groundwater Quality**

10 Groundwater quality impacts could result from (1) project construction practices, (2) the migration
11 of existing groundwater contaminant plumes toward supply wells due to changes in groundwater
12 flow paths occurring during project construction and/or operations, and/or (3) the inducement of
13 the migration of poorer-quality (higher-saline) water into the areas of higher-quality groundwater.
14 GAMA-Geotracker is a database maintained by the State of California that identifies contamination
15 sites. Figure 8-8 shows the location of identified groundwater plumes in the study area; more
16 information regarding these sites can be found in Chapter 25, *Hazards, Hazardous Materials, and*
17 *Wildfire*. Additionally, Figures 8B-3 through 8B-11 in Appendix 8B, *Impact Analysis: Groundwater*
18 *Model Results*, show the locations of these identified groundwater plumes relative to anticipated
19 changes in groundwater elevations resulting from project operation under each project alternative.



1
2

Figure 8-8. Location of Identified Groundwater Plumes in the Study Area

1 As described in Chapter 25, *Hazards, Hazardous Materials, and Wildfire*, a preliminary search of
2 government databases was conducted to identify Cortese (i.e., state-identified hazardous waste)
3 sites within 0.25 mile of project facilities. The following lists summarizes the relevant content in
4 Tables 25-1 through 25-5.

- 5 • Eight listed sites are within 0.25 mile of the intakes and North Tunnels between the intakes and
6 Twin Cities Complex, all of which have been treated and are closed.
- 7 • Seven listed sites are within 0.25 mile of the eastern alignment; of these, three sites have been
8 treated and are closed and two are undergoing remediation for soil and water contamination
9 with total petroleum hydrocarbons. Additionally, the Stockton Naval Communication Station is
10 within both the eastern alignment (Alternatives 3, 4a, 4b, and 4c) and the Bethany Reservoir
11 alignment (Alternative 5) and is discussed under Bethany Reservoir Alignment in Chapter 25.
- 12 • Eight listed sites are within 0.25 mile of the Southern Complex; of these three sites have been
13 treated and are closed and five have been designated as cleanup program sites/voluntary
14 cleanup sites. Of these five, at least one has ongoing remediation work for soil and groundwater
15 contamination.
- 16 • Seven listed sites are within the Bethany Reservoir alignment. Of these, four sites are closed and
17 three are within the project footprint for Alternative 5 and involve petroleum/gasoline leaks
18 that contaminated both soil and groundwater. The three sites are near project facilities:
19 proposed utility line, supervisory control and data acquisition (SCADA) fiber line route, and
20 levee access road and, as such, are not expected to be affected by changes in groundwater
21 elevations. Similarly, one additional site, the Stockton Naval Communications Station, has
22 ongoing remediation for soil and groundwater contamination; however, this site is within the
23 project footprint for SCADA fiber routes on Rough and Ready Island and would not involve
24 groundwater exposure or management.

25 ***All Project Alternatives***

26 As noted in Impact GW-2, changes in groundwater elevations as simulated during project operations
27 exceed 5 feet less than 1% of the time over the 94-year simulation period and occur over a very
28 small area of the model under all alternatives. However, near the groundwater plume sites shown in
29 Figure 8-8, changes in groundwater elevations are limited to 1 to 2 feet between the baseline and
30 alternatives, which is unlikely to cause a change in groundwater flow paths. Figures 8B-3 through
31 8B-11 in Appendix 8B show the locations of these identified groundwater plumes relative to
32 anticipated changes in groundwater elevations resulting from project operation under each project
33 alternative.

34 ***Project Construction***

35 The potential for project construction activities to result in groundwater contamination is addressed
36 in Chapter 25 under Impact HAZ-1: *Create a Substantial Hazard to the Public or the Environment*
37 *through the Routine Transport, Use, or Disposal of Hazardous Materials*. Additionally, groundwater
38 removed with the dewatering system would be treated as necessary, stored, and reused for water
39 supply on-site (see Chapter 3, *Description of the Proposed Project and Alternatives*). If the total
40 volume of on-site water flows, including treated dewatering flows, exceed the on-site storage and
41 water demands, water would be discharged in accordance with the Stormwater Pollution
42 Prevention Plan described in Appendix 3B, *Environmental Commitments and Best Management*
43 *Practices*. Use of slurry walls to minimize dewatering flows would minimize the volume of water to

1 be removed from the groundwater, as described above and in the Engineering Project Reports
2 (Delta Conveyance Design and Construction Authority 2022a, 2022b). As such, there would be no
3 adverse effect.

4 As previously described under Impact GW-2, project construction under all project alternatives may
5 result in changes to groundwater levels in the immediate area of the constructed facilities.
6 Dewatering of the tunnel shafts would occur for a few weeks following isolation of the shaft from
7 adjacent groundwater within the slurry wall and completed tunnel shaft. Dewatering of the
8 Southern Forebay Emergency Spillway adjacent to Italian Slough would occur over a few months.
9 Dewatering would also occur for a few months at the Southern Forebay Outlet Structure, the
10 California Aqueduct Control Structure, and the South Delta Outlet and Control Structure (for
11 Alternatives 1, 2a, 2b, 2c, 3, 4a, 4b, and 4c), and the Delta-Mendota Control Structure (for
12 Alternatives 2a and 4a). Dewatering at the intakes would occur within a slurry wall throughout most
13 of the construction period. However, monitoring for impacts from, and adaptive management of,
14 dewatering, including the potential implementation of Mitigation Measure GW-1: *Maintain*
15 *Groundwater Supplies in Affected Areas*, would avoid excessive reductions in groundwater elevations
16 on the surrounding aquifer. Impacts on groundwater elevations, and therefore groundwater
17 hydraulic gradients, as a result of project construction are anticipated to be localized and short-term
18 in nature and are not anticipated to result in significant impacts on groundwater levels. As such, the
19 change in groundwater hydraulic gradients resulting from changes in groundwater levels are not
20 likely to mobilize existing contaminant plumes in groundwater. Furthermore, Mitigation Measure
21 HAZ-2: *Perform a Phase I Environmental Site Assessment Prior to Construction Activities and*
22 *Remediate If Necessary*, would identify if there is existing groundwater contamination at a site on or
23 within 0.25 mile of the project alignment. Based on this information, additional actions, such as
24 changes to pumping and/or recharge locations and rates under Mitigation Measure GW-1 can be
25 assessed and modified, if needed, to mitigate the potential for plume migration, further limiting the
26 likely impacts of plume mobilization. Since pumped groundwater would be recharged immediately
27 outside the slurry walls through Mitigation Measure GW-1 as needed, no significant regional
28 changes in groundwater flow directions are anticipated and the inducement of poor-quality
29 groundwater into areas of better quality is unlikely. It is therefore anticipated that there would be
30 no significant change in groundwater quality as a result of project construction.

31 Finally, practices for minimizing construction-related impacts to groundwater quality can be found
32 in Appendix 3B, *Environmental Commitments and Best Management Practices*. These practices
33 employed during construction would minimize or eliminate potential impacts such that there would
34 be no significant change in groundwater quality as a result of project construction.

35 Operations

36 Similar to project construction, the potential for project operations and maintenance activities to
37 result in groundwater contamination is addressed in Chapter 25 under Impact HAZ-1. Dewatering of
38 the sedimentation basins at the intakes during project maintenance would occur rarely and only if
39 non-periodic structural repairs were needed. During annual removal of sediment, the sedimentation
40 basin would not need to completely be drained. Water removed during the infrequent dewatering
41 would probably occur for a brief time and the flows would be tested and discharged into the tunnel.
42 Groundwater management practices associated with infrequent dewatering during project
43 maintenance for structural repairs to the sedimentation basins are similar to those that would be
44 conducted during project construction and would also minimize dewatering impacts to the extent
45 practicable, as described in the Engineering Project Reports, resulting in no adverse effects from

1 project operations and/or maintenance (Delta Conveyance Design and Construction Authority
2 2022a, 2022b).

3 Project operation and maintenance under all alternatives would occur within the same footprint as
4 construction. As noted in Chapter 25, project operations and maintenance activities would occur
5 after identified Cortese sites were evaluated and, if needed, remediated. Therefore, the risk to
6 expose the environment to hazardous materials from a known Cortese site is low. Similarly, as
7 demonstrated through the simulation of project operations under all alternatives, groundwater level
8 impacts would occur in the upper three model layers, extending from the ground surface to a depth
9 of around 165 feet bgs. Model results show that groundwater elevation declines of greater than 5
10 feet occur less than 1% of the time or 1 year of the 94-year simulation period from 1922 to 2015.
11 Groundwater elevation changes near active contamination sites identified in Figure 8-8 never
12 exceed 1 to 2 feet. Therefore, the likelihood of plume mobilization as a result of changes in
13 groundwater elevations is considered to be less than significant. Contour maps of maximum
14 groundwater elevation changes are presented in Appendix 8B.

15 Finally, similar to construction dewatering, maintenance dewatering near the intake facilities would
16 temporarily lower groundwater levels and cause small changes in groundwater flow patterns near
17 the study area. Groundwater elevations outside the slurry walls would be monitored and
18 dewatering operations would be managed. If required, Mitigation Measure GW-1 would be
19 implemented, recharging dewatering flows immediately outside the slurry walls, to manage impacts.
20 As such, no significant regional changes in groundwater flow directions are anticipated and the
21 inducement of poor-quality groundwater into areas of better quality is unlikely. Therefore, it is
22 anticipated that there would be no change in groundwater quality as a result of project operations
23 and/or maintenance.

24 ***CEQA Conclusion—All Project Alternatives***

25 Significant impacts on groundwater quality as a result of project construction are not anticipated as
26 construction-related practices and BMPs would minimize the potential for water quality impacts.
27 Because of the temporary and localized nature of construction dewatering, the potential for the
28 inducement of the migration of poor-quality groundwater into areas of higher quality groundwater
29 would be low, and similarly, the likelihood of the inducement of the migration of existing
30 contaminant plumes in groundwater would be low. Further, the planned treatment of extracted
31 groundwater prior to reuse, storage, and possible discharge into adjacent surface waters and/or to
32 land would prevent significant impacts on groundwater quality.

33 No significant groundwater quality impacts are anticipated in and adjacent to the project alignment
34 due to project operations because significant changes to regional patterns of groundwater flow are
35 not anticipated. Additionally, project operations and maintenance activities would follow BMPs,
36 minimizing any impacts relating to spills or other occurrences that could affect groundwater quality.
37 This impact would be less than significant.

38 ***Mitigation Impacts***

39 ***Compensatory Mitigation***

40 Although the CMP described in Appendix 3F does not act as mitigation for impacts on this resource
41 from project construction or operations, its implementation could result in groundwater quality
42 impacts.

1 Under the CMP, wetlands and other habitats would be created on Bouldin Island, at the I-5 ponds
2 (Ponds 6, 7, and 8), and in the North Delta Arc and would not be expected to directly affect
3 groundwater quality. Additionally, the increased groundwater levels from the habitat creation may
4 result in a westward groundwater hydraulic gradient, a project benefit that would reduce the
5 potential for saltwater movement from Delta waters into the underlying groundwater basins around
6 the intake areas. As such, with implementation of the CMP, there would be little to no impact on
7 groundwater quality. Implementation of compensatory mitigation would not change the overall
8 impact conclusion of less than significant.

9 Other Mitigation Measures

10 Some mitigation measures would involve providing new water wells or relocating and/or replacing
11 wells, pipes, power lines, drainage systems, and other infrastructure that would have the potential
12 to degrade groundwater quality. The mitigation measure with potential to result in degradation of
13 groundwater quality is Mitigation Measure AG-2: *Replacement or Relocation of Affected*
14 *Infrastructure Supporting Agricultural Properties*. Temporary groundwater quality degradation
15 resulting from mitigation measures would be similar to construction effects of the project
16 alternatives in certain construction areas and would contribute to groundwater quality impacts of
17 the project alternatives. Groundwater removed with the dewatering system would be treated as
18 necessary prior to reuse, storage, and possible discharge. Water would be discharged in accordance
19 with the Stormwater Pollution Prevention Plan Because of the temporary and localized nature of
20 construction dewatering, the potential for migration of poor-quality groundwater into areas of
21 higher-quality groundwater would be low, and similarly, the likelihood of migration of existing
22 contaminant plumes in groundwater would be low. Therefore, other mitigation measures are
23 unlikely to result in the degradation of groundwater quality and the impact of groundwater quality
24 would not be substantial.

25 Overall, the impact of degradation of groundwater quality from construction of compensatory
26 mitigation and implementation of other mitigation measures, combined with project alternatives,
27 would not change the less-than-significant impact conclusion.

28 **8.3.3 Cumulative Analysis**

29 Cumulative effects result from incremental impacts of a proposed project when added with other
30 past, present, and reasonably foreseeable future projects. This section identifies the potential for
31 past, present and reasonably foreseeable future programs, projects, and policies to cause adverse
32 cumulative impacts on groundwater resources.

33 When the effects of any of the project alternatives are considered in combination with the effects of
34 initiatives listed in Table 8-10, the cumulative effects on groundwater resources could be adverse.
35 The specific programs, projects, and policies are identified below based on the potential to
36 contribute to an impact on groundwater identified under a project alternative that could be deemed
37 cumulatively considerable. The potential for cumulative impacts on groundwater resources is
38 described for effects related to the construction of water conveyance facilities and effects stemming
39 from the long-term implementation of the proposed project alternatives.

40 The list presented in Table 8-10 includes projects considered for this cumulative effects section; for
41 a complete list of such projects, consult Appendix 3C, *Defining Existing Conditions, No Project*
42 *Alternative, and Cumulative Impact Conditions*. Several projects that are included in Table 3C-3 for

1 the cumulative impact assessment might have had construction impacts on groundwater resources,
 2 but they have been completed and therefore were not included in this analysis.

3 **Table 8-10. Cumulative Impacts on Groundwater from Plans, Policies, and Programs**

Program/Project	Agency	Status	Description of Program/Project	Effects on Groundwater Resources
North Delta Flood Control and Ecosystem Restoration Project	DWR	Final EIR completed in 2010.	Project implements flood control and ecosystem restoration benefits in the north Delta (California Department of Water Resources 2007).	Potential increase in groundwater levels and groundwater recharge; potential groundwater seepage to adjacent islands/tracts; potential groundwater contamination
Dutch Slough Tidal Marsh Restoration Project	DWR	Final EIR completed in 2010. Supplemental EIR completed in 2014.	Project includes breaching levees and restoring a tidal channel system on parcels between Dutch Slough and Contra Costa Canal (California Department of Water Resources and California State Coastal Conservancy 2014).	Potential groundwater intrusion onto adjacent parcels.
Los Vaqueros Reservoir Expansion Project	CCWD, Reclamation, and DWR	Final EIS/EIR completed in 2010 with Final Supplement completed in 2020. Final feasibility report completed in 2020.	Project will increase the storage capacity of Los Vaqueros Reservoir and divert additional water from the Delta.	Construction of the first phase was completed in 2012 (raising the dam height by 34 feet). The second phase has been evaluated in an environmental impact report/environmental impact statement that indicates no adverse effects or less-than-significant effects on groundwater resources.
Eastern San Joaquin Integrated Conjunctive Use Program	Northeastern San Joaquin County Groundwater Banking Authority	Final Programmatic EIR completed in 2011.	Program will improve the use and storage of groundwater by implementing conjunctive use projects such as water transfers and groundwater banking.	Affect groundwater level fluctuations due to groundwater banking operations; potential groundwater quality impacts; mostly beneficial effects; the effects would be located outside of the action alternatives conveyance footprint area
Grassland Bypass Project	Reclamation, San Luis & Delta-Mendota Water Authority	Final EIS/EIR completed in 2009.	Reduce effects from agricultural drainage on wildlife refuges and wetlands. Will convey subsurface agricultural drainage to Mud Slough (tributary of San Joaquin River) (Bureau of Reclamation and San Luis and	Beneficial, neutral, or less-than-significant effects on subsurface agricultural drainage and shallow groundwater levels; beneficial effects on groundwater salinity

Program/Project	Agency	Status	Description of Program/Project	Effects on Groundwater Resources
			Delta-Mendota Water Authority 2009:ES-2).	
San Joaquin River Restoration Program	Reclamation, USFWS, NMFS, DWR, and CDFW	Final EIS/EIR completed in 2012.	The San Joaquin River Restoration Program is a direct result of a September 2006 legal settlement by the U.S. Departments of the Interior and Commerce, the Natural Resources Defense Council, and the Friant Water Users Authority to restore spring and fall run Chinook salmon to the San Joaquin River below Friant Dam while supporting water management actions within the Friant Division. Public Law 111-11 authorized and directed federal agencies to implement the settlement. Interim flows began October 1, 2009, and full restoration flows are scheduled to begin no later than January 2014. Site-specific improvements are ongoing.	Temporary construction-related effects on groundwater quality; changes in groundwater levels and groundwater quality along San Joaquin River; changes in groundwater levels and groundwater quality in CVP/SWP service areas
California EcoRestore	DWR, Delta Conservancy, various other state and local agencies, NGOs, and private sector partners	Initiated in 2015.	This program will accelerate and implement a suite of Delta restoration actions for up to 30,000 acres of fish and wildlife habitat by 2020. Construction of improvements is ongoing.	Potential for direct and indirect effects on groundwater conditions adjacent to tidal habitat restoration sites.
SGMA Implementation	DWR (in collaboration with State Water Resources Control Board)	Signed into law September 2014.	Defines rules and regulations that DWR needs to implement to help local agencies manage groundwater resources sustainably. GSPs for critically overdrafted groundwater basins were submitted to DWR by January 31, 2020.	The SGMA requires the formation of locally controlled GSAs, which must develop GSPs in groundwater basins or subbasins that DWR designates as medium or high priority. This will have a beneficial effect on groundwater resources, as most areas will manage groundwater extractions to not exacerbate further groundwater level declines.
San Francisco Bay Area Integrated Regional Water Management Plan	Bay Area Water Quality and Supply Reliability Program	Final Released September 2013.	The Bay Area Integrated Regional Management Plan is an evolving plan that will be used to prioritize projects and provide information for projects to be	Program identifies local water supply projects to increase water supply reliability in the Bay Area, including for SWP

Program/Project	Agency	Status	Description of Program/Project	Effects on Groundwater Resources
			funded by state and federal agencies, such as the Proposition 50 and Proposition 1 projects.	and CVP water users. One of the identified goals is for better conjunctive use and groundwater management. This would have a beneficial effect on groundwater resources.
Sacramento River Water Reliability Study	Placer County Water Agency	Notice of Preparation in 2003. Project is on hold during recent recession. Reclamation was preparing a joint NEPA document; however, the NEPA process was halted in 2009. The study has been suspended.	Placer County Water Agency, Sacramento Suburban Water District, and the cities of Roseville and Sacramento, are investigating the viability of a joint water supply diversion from the Sacramento River, consistent with the Water Forum Agreement to meet planned future growth within the Placer-Sacramento region, maintain reliable water supply while reducing diversions of surface water from the American River in future dry years to preserve the river ecosystem, and enhance groundwater conjunctive management to help sustain the quality and availability of groundwater.	Outcomes of this study could help with improved groundwater and management in the region and reduced impacts on groundwater levels and quality.
Harvest Water	Sacramento Regional County Sanitation District	Project is currently in design. All CEQA documentation is complete.	Harvest Water is being developed by Regional San and has the potential to deliver up to 50,000 AFY of drought-resistant recycled water to irrigate more than 16,000 acres of permanent agriculture and habitat conservation lands near the Cosumnes River and Stone Lakes Wildlife Refuge. This recycled water would be used in-lieu of pumping groundwater. Additionally, Harvest Water proposes wintertime irrigation and wildlife-friendly recharge basins in the study area where the soils are suitable, to provide further groundwater recharge.	Project will offset groundwater use in the area near the intake facilities, helping the groundwater basin move toward and manage for groundwater sustainability and increasing groundwater levels.
In-Delta Storage Project (Delta Wetlands Project)	DWR and Reclamation	Draft Supplemental Report to 2004 Draft State Feasibility Study In-Delta	The In-Delta Storage Project, described in the 2004 Draft State Feasibility Study, would store about 217,000 AF of water in the south Delta for a wide array of water supply, water	Project is inconsistent with Contra Costa County General Plan Policy for Agricultural Lands and Delta Protection Commission's

Program/Project	Agency	Status	Description of Program/Project	Effects on Groundwater Resources
		Storage Project completed in 2006.	quality, and ecosystem benefits. The project would consist of two reservoir islands (Webb Tract and Bacon Island), two habitat islands (Holland Tract and Bouldin Island) and four integrated facilities (two facilities on each of the storage islands). Water storage would be created on the islands by strengthening existing levees and building new embankments inside the existing levees. The integrated facilities would control water diversions and releases into and out of the reservoir islands. The facilities control structures would be consolidated to combine all operational components needed to make diversions and releases. The components of each facility would include a fish screen, a transition pool, three inlet/outlet structures, a midbay, a pumping plant and associated conduit, a bypass channel and engineered embankments. This project has been re-defined under the Delta Wetlands Project	Land Use Plan Principles for Agriculture and Recreation. Project will also result in conversion of existing agricultural land. Reservoir islands might affect shallow groundwater levels and agricultural drainage patterns.
Shasta Lake Water Resources Investigation	Reclamation	Final EIS completed in 2015. Final Feasibility report completed in 2020.	The project is a multipurpose plan to modify Shasta Dam and Reservoir to increase survival of anadromous fish populations in the upper Sacramento River; increase water supplies and water supply reliability; and, to the extent possible through meeting these objectives, include features to benefit other identified ecosystem, flood damage reduction, and related water resources needs which could result in additional storage capacity of 256,000 to 634,000 AF.	Program identifies water supply plans to maintain and possibly increase water supply reliability for CVP water users, which would indirectly benefit groundwater resources by helping reduce the amount of groundwater that needs to be pumped for agricultural irrigation.
North-of-the-Delta Offstream Storage Investigation	DWR and Reclamation	Draft EIR/EIS completed in 2017. Summary of project description information	The plan will provide offstream storage in the northern Sacramento Valley for improved water supply and water supply reliability, improved water quality, and enhanced survival of anadromous fish and other	Program identifies water supply plans to maintain and possibly increase water supply reliability for CVP and non-CVP water users. This would help with decreasing the

Program/Project	Agency	Status	Description of Program/Project	Effects on Groundwater Resources
		released in 2021.	aquatic species. All alternatives include a new reservoir at the Sites location, with various facilities for water conveyance.	reliance on groundwater supply in dry years.
Upper San Joaquin River Basin Storage Investigation	Reclamation	Draft EIS published in August 2014.	The Upper San Joaquin Storage would contribute to restoration of the San Joaquin River, improve water quality of the San Joaquin River, and facilitate additional conjunctive management and water exchanges that improve the quality of water deliveries to urban communities.	Program identifies water supply plans to maintain and possibly increase water supply reliability for CVP and non-CVP water users. This would help with decreasing the reliance on groundwater supply in dry years in the export service areas within the San Joaquin and Tulare groundwater basins.
Riverside-Corona Feeder Conjunctive Use Project	Western Municipal Water District and Reclamation	Final Supplemental EIS and EIR published in 2011. Final Supplemental EIR/EIS completed in 2012.	The project would allow WMWD to purchase water from SWP and store up to 40,000 AF of water in the San Bernardino basin area and Chino basin and to extract the water from the groundwater basins. The facilities would convey local water supplies and deliver treated imported water.	Program would maintain and possibly increase water supply reliability for SWP water users, especially in drier years. This program would allow for better conjunctive use and management.
Seawater Desalination Project at Huntington Beach	Metropolitan Water District of Orange County	Final Subsequent EIR completed in 2010. Awaiting permits.	Water treatment plant would provide up to 50 million gallons per day of desalinated water.	Program would maintain and possibly increase water supply reliability for SWP water users. This would help with decreasing the reliance on groundwater supply.
Carlsbad Seawater Desalination Plant	San Diego County Water Authority and other water suppliers	Desalination plant is currently operating.	Water treatment plant provides up to 50 million gallons per day of desalinated water.	Program would maintain and possibly increase water supply reliability for SWP water users. This would help with decreasing the reliance on groundwater supply.
Emergency Storage Project	San Diego County Water Authority	Project is operational.	The project will increase the amount of water stored locally. New water storage and pipeline connections distributes water throughout the region if imported water supplies are reduced. The Emergency Storage Project is expected to meet the county's emergency water needs through 2030.	Program would maintain and possibly increase water supply reliability for SWP water users. This would help with decreasing the reliance on groundwater supply.
Del Puerto Canyon Reservoir	San Joaquin River Exchange	Final EIR was certified in 2020 but a	DPWD and the Exchange Contractors are partnering to construct and operate the Del	Project will provide additional surface water to offset current

Program/Project	Agency	Status	Description of Program/Project	Effects on Groundwater Resources
	Contractors Water Authority, Del Puerto Water District	CEQA lawsuit filed. The Bureau of Reclamation is currently working on an EIS. Design is pending.	Puerto Canyon Reservoir, an 800-acre reservoir that would store up to 82,000 AF of water. The project will deliver water from the Delta-Mendota Canal into the new reservoir, where it will be stored and released on a carefully managed basis. The reservoir would allow water to be delivered into storage during wetter periods until it is needed in drier periods for irrigation, groundwater recharge, or wildlife beneficial uses (up to 60,000 AFY).	groundwater use in the Delta-Mendota groundwater subbasin. Project may increase water supply reliability for CVP water users, which would indirectly benefit groundwater resources by helping reduce the amount of groundwater that needs to be pumped for agricultural irrigation
San Luis Reservoir Expansion	Reclamation	Draft Appraisal Report published in December 2013. Final Supplemental Environmental Impact Statement completed in 2020.	The plan is to increase the storage capacity of San Luis Reservoir (behind B.F. Sisk Dam) to improve the reliability of CVP and SWP water supplies dependent upon San Luis Reservoir. Seismic risks under the dam and in the Delta, regulatory constraints to operating Delta export facilities, algae blooms at low water levels, and future climate change have and will reduce the reliability of CVP/SWP deliveries dependent upon the San Luis Reservoir.	Program identifies water supply plans to maintain and possibly increase water supply reliability for CVP and SWP water users. This would help with decreasing the reliance on groundwater supply.
South Delta Temporary Barriers Project	DWR	Ongoing Program. Comprehensive Operations Plan and Monitoring Special Study released in 2019.	The program was initiated in 1991 and includes four rock barriers across South Delta channels. The objectives of the project are to increase water levels, improve water circulation patterns and water quality in the southern Delta for local agricultural diversions, and improve operational flexibility of the SWP to help reduce fishery impacts and improve fishery conditions.	Program identifies water supply plans to maintain water supply reliability for CVP and SWP water users. This would help with decreasing the reliance on groundwater supply.
Implementation of Senate Bill X7 7	DWR	Legislation was adopted in 2009.	This legislation requires the state to achieve a 20% reduction in urban per capita water use by December 31, 2020; require each urban retail water supplier to develop urban water use targets; agricultural water suppliers to implement efficient water management practices; and DWR in consultation with other state agencies, to develop	The legislation would reduce water demands for existing water users; and reduce projected demands for future growth.

Program/Project	Agency	Status	Description of Program/Project	Effects on Groundwater Resources
			a single standardized water use reporting form.	
Irrigated Lands Regulatory Program	Central Valley Regional Water Quality Control Board	Program began in 2003 to prevent agricultural runoff from impairing surface waters, and in 2012, groundwater regulations were added to the program.	This program regulates discharges from irrigated agricultural lands. Its purpose is to prevent agricultural discharges from impairing the waters that receive the discharges. The California Water Code authorizes State and Regional water boards to conditionally waive waste discharge requirements if this is in the public interest. On this basis, the Los Angeles, Central Coast, Central Valley, and San Diego regional water quality control boards have issued conditional waivers of waste discharge requirements to growers that contain conditions requiring water quality monitoring of receiving waters. Participation in the waiver program is voluntary; dischargers must file a permit application as an individual discharger, stop discharging, or apply for coverage by joining an established coalition group. The waivers must include corrective actions when impairments are found.	Reduces the potential for groundwater contamination from agricultural practices.
Bay-Delta Water Quality Control Plan Update	State Water Resources Control Board	Ongoing development.	The State Water Resources Control Board is updating the 2006 Bay-Delta WQCP in four phases: Phase I: Modifying water quality objectives (i.e., establishing minimum flows) on the Lower San Joaquin River and Stanislaus, Tuolumne, and Merced Rivers to protect the beneficial use of fish and wildlife and (2) modifying the water quality objectives in the southern Delta to protect the beneficial use of agriculture; Phase II: Evaluating and potentially amending existing water quality objectives that protect beneficial uses and the program of implementation to achieve those objectives. Water	Water supplies of water rights users and SWP and CVP water users could be affected if increased instream flow and/or Delta outflow objectives are established in the regulatory process to protect beneficial uses. This could result in increased groundwater pumping and decreased groundwater levels in some areas.

Program/Project	Agency	Status	Description of Program/Project	Effects on Groundwater Resources
			quality objectives that could be amended include Delta outflow criteria; Phase III: Requires changes to water rights and other measures to implement changes to the WQCP from Phases I and II; Phase IV: Evaluating and potentially establishing water quality criteria and flow objectives that protect beneficial uses on tributaries to the Sacramento River.	
Southport Sacramento River Early Implementation Project	USACE	Final EIS issued May 2015.	This project would implement flood risk-reduction measures along the Sacramento River South Levee in the city of West Sacramento, Yolo County, California. The area of flood risk-reduction measure implementation extends along the right (west) bank of the Sacramento River south of the Barge Canal downstream 5.6 miles to the South Cross Levee, adjacent to the Southport community of West Sacramento.	Significant impacts on groundwater could result from construction dewatering activities; these impacts would be reduced to a less-than-significant level with the implementation of groundwater well protection measures during construction.

1 AFY= acre-feet per year; CCWD = Contra Costa Water District; CDFW = California Department of Fish and Wildlife; CEQA
 2 = California Environmental Quality Act; CVP = Contra Valley Project; DPWD = Del Puerto Water District; DWR =
 3 California Department of Water Resources; EIR = environmental impact report; EIS = environmental impact statement;
 4 GSA= groundwater sustainability agency; GSP = Groundwater Sustainability Plans; NEPA = National Environmental
 5 Policy Act; NMFS = National Marine Fisheries Service; Reclamation = U.S. Bureau of Reclamation; SGMA = Sustainable
 6 Groundwater Management Act; SWP = State Water Project; USACE = U.S. Army Corps of Engineers; USFWS = U.S. Fish
 7 and Wildlife Service; WMWD = Western Municipal Water District; WQCP = Water Quality Control Plan.
 8

9 **8.3.3.1 Cumulative Impacts of the No Project Alternative**

10 The cumulative No Project Alternative scenario would include projects listed in Table 8-10 and
 11 could have effects on groundwater resources. Generally, these projects in the study area would have
 12 positive effects on the underlying groundwater basins on a long-term basis, but could have potential
 13 negative effects during construction. However, construction effects would likely be short-term in
 14 duration. The No Project Alternative scenario may also put additional strains on water resources
 15 that may include an increase in demand for groundwater to meet future water needs. However,
 16 medium and high priority basins are subject to SGMA and projects listed in Table 8-10 would also
 17 have to undergo independent environmental analysis. Therefore, it is anticipated that there would
 18 be no cumulative impact on groundwater resources under the No Project Alternative.

19 **8.3.3.2 Cumulative Impacts of the Project Alternatives**

20 The projects listed in Table 8-10 could occur along with construction of the Delta Conveyance
 21 Project. As presented before, groundwater impacts associated with the project alternatives are

1 similar to one another. The projects listed in Table 8-10 also would have to undergo independent
2 environmental analysis and comply with SGMA. Simultaneous construction of the Delta Conveyance
3 Project and other projects in the vicinity of the project could potentially result in significant impacts
4 on groundwater if construction BMPs and compensatory mitigation are not implemented.

5 Potential project impacts would be predominantly realized through the routine transport, use, or
6 disposal of hazardous materials, the release of hazardous materials into the environment, or
7 significant changes in groundwater gradients that result in the movement of existing groundwater
8 contamination plumes. However, impacts from minor spills or drips would be avoided by
9 thoroughly cleaning up minor spills as soon as they occur, by monitoring groundwater levels for
10 adverse effects during construction, and by the recharge of groundwater extracted as part of
11 dewatering operations during construction, which would minimize the potential for resultant plume
12 movement. While foreseeable projects have the potential to cause similar impacts, it is assumed
13 these projects would also implement similar construction BMPs and follow all regulations regarding
14 the transport, disposal, and handling of hazardous wastes during construction. Furthermore, as the
15 project results in the remediation and cleanup of certain hazardous sites and locations in the study
16 area, groundwater quality conditions would improve. Therefore, all project alternatives would not
17 result in an incremental cumulatively considerable impact.

18 The simultaneous operation of the Delta Conveyance Project along with projects listed in Table 8-10
19 are anticipated to have more beneficial impacts on groundwater than adverse for all alternatives.
20 Most of the projects in Table 8-10 focus on the development of surface water supplies that would
21 offset groundwater use and improve the reliability of local water supplies and SWP/CVP deliveries,
22 thereby reducing stresses and demands on the local groundwater systems. Additionally, the
23 availability and use of more reliable surface water supplies would result in increased groundwater
24 percolation and recharge, raising groundwater levels. The increased reliability of CVP and SWP
25 supplies would allow GSAs charged with managing the long-term sustainability of groundwater
26 basins, along with water agencies, to improve the conjunctive use of their surface water and
27 groundwater supplies and reduce stress on the underlying groundwater basins. Cumulative effects
28 on groundwater supplies described in previous sections are expected to be mostly positive, with
29 some effects negligible or less than significant under all project alternatives and are therefore
30 anticipated to have less-than-significant cumulative impacts in the region.